

Preliminary Stormwater Management Report

Wawa – Store #TBD Franklin, IN

Date Prepared: 12/3/2024

Revised:

On behalf of:



Contact:

Paul Hanson paul.hanson@cesoinc.com 618.604.7157

CESO 7777 Bonhomme Ave, Suite 1853, Clayton MO 63105

Engineer of Record:



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Introduction

This report covers the methodology and calculations used in the design of the stormwater management system for the proposed development anticipated for the Northeast Highway 31st & East County Road 300 North (Earlywood Drive), Franklin, IN 46131.

The stormwater management system is designed in accordance with the City of Franklin, Indiana Code of Ordinances Chapter 16.28.190 General Drainage Standards and INDOT requirements to accommodate the release rate requirements and the water quality volume requirements.

- Per the City of Franklin, Indiana Code of Ordinances, the 10-year post developed release rate must be reduced to the 2-year pre-developed release rate and the 100-year post developed release rate must be reduced to the 10-year pre-developed release rate.
- Per the City of Franklin, Indiana Code of Ordinances, the water quality volume requirement can be satisfied by designing a post construction BMP that is sized to treat the water quality volume for this site. Per the City of Franklin, Indiana Code of Ordinances, the developer shall be required to provide a water quality detention system that is designed to detain, for over 24 hours after peak run off from a 24-hour storm, at least 20% of the runoff from either a one and one-fourth inch storm or one-half inch of direct-runoff, whichever is greater. All paved areas shall be routed through a water quality detention area, with the minimum water quality outlet being two inches in diameter.

Storm routings for this project were performed using HydroCAD. Time of Concentration was determined using TR-55 method, within HydroCAD. The critical storm was determined using the HUFF method in HydroCAD.

Stormwater quality volume calculations were performed using HydroCAD. Refer to Appendix D for water quality calculations.

The onsite soils were obtained from USDA NRCS Web Soil Survey and can be found in Appendix E.

Existing Conditions

The site is a 10.0 Ac.± existing open field. There is a farm dealer located to the North, a private school to the East, a car dealership to the South, and Highway 31st to the West.

The existing runoff consists of two (2) major drainage areas as listed below:

- Pre-Developed Northwest Drainage Area (1A)- This drainage area drains to the Northwest portion of the site to the existing headwall and continues offsite to the North property.
- Pre-Developed Southeast Drainage Area (1B)- This drainage area drains to the southeast portion of the site, to an existing headwall and continues offsite to the East property.



The soil survey indicates the site to have Brookston Silty Clay Loam (Br), Hydrological Soil Group 'D' type soil, Crosby Silt Loam (CrA), Hydrological Soil Group 'D' type soil, Urban Land-Brookston Complex (UbaA), Hydrological Soil Group 'D', Urban Land-Crosby Silt Loam Complex (UcfA), Hydrological Soil Group 'D', and Crosy Silt Loam (YcIA), Hydrological Soil Grop 'D'. We assumed a CN value of 80 for Hydrological Soil Group D. We assumed the grass areas to be in good condition.

Please refer to Appendix B for Pre- and Post-Developed Drainage Plans.

Peak runoff rates from the existing conditions are listed in the following table:

Existing Conditions Peak Runoff Rates									
Drainage Area 2-year Storm 10-year Storm 100-year storm									
1A	<mark>1.43</mark>	<mark>4.25</mark>	12.55						
1B	0.22	<mark>0.65</mark>	1.91						

Proposed Conditions

The proposed development of the site will consist of the construction of a 6,372 SF building, auto-fueling canopy, a paved parking area, paved drive aisles, associated site improvements, and two stormwater management systems. The stormwater management systems consist of two wet detention basins, associated outlet control structures, and emergency spillways. The wet detention basins in conjunction with the outlet control structures have been designed to address water quality requirements. The outlet from the stormwater management system will be routed through the outlet control structure and route to the existing outfall point to the Northwest and Southeast. Please refer to Appendix A for a detailed Site Plan for the proposed development.

The proposed improvements will create two (4) major drainage areas, (2) detention nodes, and (2) Final Outfall nodes as listed below:

- Post-Developed Northwest Drainage Area (Detained) (2A) This drainage area drains toward the proposed North detention basin.
- Post-Developed Northwest Drainage Area Direct Runoff (3A) This drainage area is undetained and drains to the Northwest.
- North Basin (4A)- North basin detention node.
- Final Northwest Outfall (5A)- This is the final outfall to the Northwest, combining nodes 2A, 3a, and $\Delta\Delta$
- Post-Developed Southeast Drainage Area (Detained) (2B) The drainage area drains toward the proposed Southeast detention basin.
- Post-Developed Southeast Drainage Area Direct Runoff (3B) This drainage area is undetained and drains to the Southeast.
- Southeast Basin (4B) Southeast basin detention node.
- Final Southeast Outfall (5B) This is the final outfall to the Southeast, combining nodes 2B, 3b, ad 4B.

Group 'D' was used for all Hydrological soil groups. We assumed CN values of 98 for impervious and 80 for pervious areas in good condition.

Please refer to Appendix B for Pre- and Post-Developed Drainage Plans.



Stormwater Quantity Summary

Downstream flows have also been analyzed utilizing HydroCAD® 2022. Rainfall depths were obtained from Rainfall Frequency Atlas of the Midwest. A storm analysis using the Huff Method was performed to determine the critical storm. For the North basin and the Southeast basin the critical storm durations were determined to be the 30 minute storms. The times of concentration were calculated using the TR-55 method, with a minimum time of concentration of 10 minutes. The downstream flows for the post developed conditions were determined to be less than the pre-developed flows for the 10 and 100-year storm events.

The resulting proposed conditions peak run off rates are listed in the following table:

	Proposed Conditions Peak Runoff Rates											
Drainage Area	Drainage Area 2-year 10-year 100-year											
2A	5.48	10.46	21.45									
3A	0.55	1.37	3.56									
2B	1.51	2.78	5.56									
3B	0.04	0.13	0.37									

The discharge characteristics for the proposed stormwater management basin and drainage areas are listed in the following table:

	Discharge Summary									
Storm	Final Outfall Northwest Allowable Discharge (1A)	Final Outfall Northwest Discharge (5A)	Final Outfall Southeast Allowable Discharge (1B)	Final Outfall Southeast Discharge (5B)						
10-year	1.43	1.42	0.22	0.22						
100-year	4.25	3.65	0.65	0.49						

Reference Appendix C for full HydroCAD reports for each drainage area.

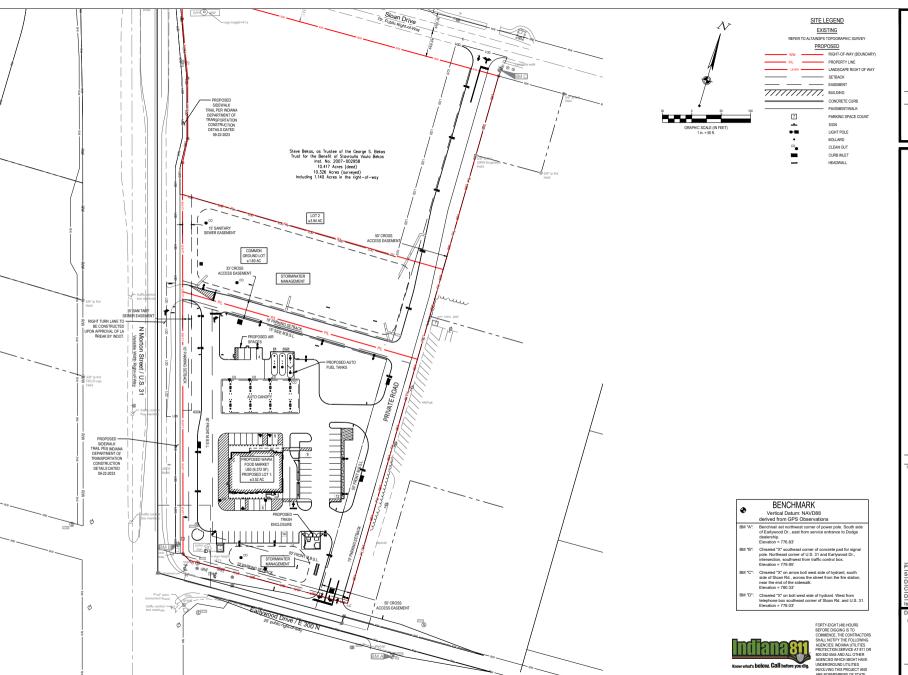
Stormwater Quality Summary

As part of the requirements from the City of Franklin, Indiana Code of Ordinances, the water quality volume requirement can be satisfied by designing a post construction BMP that is sized to treat the water quality volume for this site. Per the City of Franklin, Indiana Code of Ordinances, the developer shall be required to provide a water quality detention system that is designed to detain, for over 24 hours after peak run off from a 24-hour storm, at least 20% of the runoff from either a one and one-fourth inch storm or one-half inch of direct-runoff, whichever is greater. All paved areas shall be routed through a water quality detention area, with the minimum water quality outlet being two inches in diameter. It was determined that 20% of the 1.25-inch storm volume generated larger volumes for both the North basin and the Southeast basin. The proposed development meets the water quality requirement utilizing the wet detention basins. The outlet control structure and orifice have been sized to drain the required water quality volume within 24 hours, per the requirements.

Reference Appendix D for full Water Quality Calculations.



APPENDIX A: SITE PLANS









FRANKLIN, IN

MAWA STORY S

0 2024 CESO, INC.

Project Number: 763219

Scale: 1"=50"

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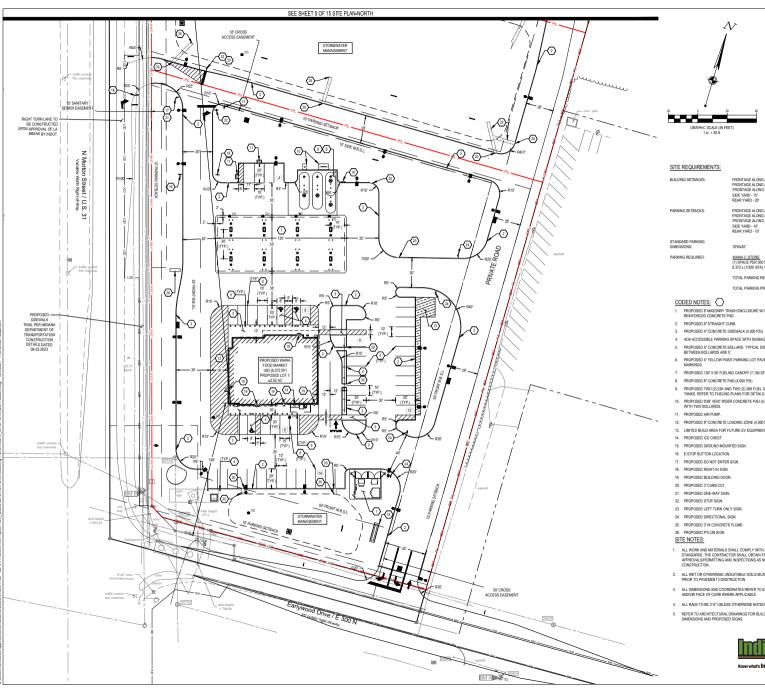
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 JTK

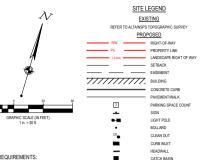
 Date:
 12/04/2024

 Issue:
 NOT FOR CONSTRUCTION

Drawing Title:

ARE NONMEMBERS OF STATE UTILITIES PROTECTION SERVICE OVERALL SITE PLAN





FRONTAGE ALONG (EAST PRIVATE ROAD) - 50' FRONTAGE ALONG (US 31 ROW) - 50' FRONTAGE ALONG (EARLYWOOD DRIVE / E 300N) - 50'

SIDE YARD - 15' REAR YARD - 20'

FRONTAGE ALONG (EAST PRIVATE ROAD) - 10'
FRONTAGE ALONG (US 31 ROW) - 10'
FRONTAGE ALONG (EARLYWOOD DRIVE / E 300N) - 10'

10Wx20"

WAWA C-STORE: (1) SPACE PER 300 S.F. OF GROSS FLOOR AREA 6,372 x (1/300 GFA) = 22 SPACES

TOTAL PARKING REQUIRED = 22 SPACES

TOTAL PARKING PROPOSED = 53 SPACES

- PROPOSED 8' MASONRY TRASH ENCLOSURE W/ 8" REINFORCED CONCRETE PAD.
- 3 PROPOSED AT CONCRETE SIDEWALK (A DDD PSI)
- 4. ADA ACCESSIBLE PARKING SPACE WITH SIGNAGE. PROPOSED 6" CONCRETE BOLLARD. TYPICAL DISTANCE
- BETWEEN BOLLARDS ARE 5'.
- 6. PROPOSED 4" YELLOW PAINT PARKING LOT PAVEMENT
- 7. PROPOSED 130' X 55' FUELING CANOPY (7,150 SF)
- 8 PROPOSED 8" CONCRETE PAD (4 000 PSI)
- PROPOSED TWO (2) 22K AND TWO (2) 20K FUEL STORAGE TANKS. REFER TO FUELING PLANS FOR DETAILS.
- 10. PROPOSED 6'X6' VENT RISER CONCRETE PAD (4,000 PSI)
- 12. PROPOSED 8" CONCRETE LOADING ZONE (4,000 PSI).
- 13. LIMITED BUILD AREA FOR FUTURE EV EQUIPMENT
- 14. PROPOSED ICE CHEST.
- 15. PROPOSED GROUND MOUNTED SIGN
- 16 F-STOP BUTTON LOCATION
- 17. PROPOSED DO NOT ENTER SIGN.
- 10 DRODOSED BLILDING DOOR
- 20. PROPOSED 3' CURB CUT.

- 23. PROPOSED LEFT TURN ONLY SIGN.

- ALL WORK AND MATERIALS SHALL COMPLY WITH ALL INDOT STANDARDS. THE CONTRACTOR SHALL OBTAIN FINAL APPROVALSPERMITTING AND INSPECTIONS AS NECESSARY PRIOR TO CONSTRUCTION.
- ALL WET OR OTHERWISE UNSUITABLE SOILS MUST BE STABILIZED PRIOR TO PAVEMENT CONSTRUCTION.
- 3. ALL DIMENSIONS AND COORDINATES REFER TO EDGE OF PAVEMENT
- AND/OR FACE OF CURB WHERE APPLICABLE.
- REFER TO ARCHITECTURAL DRAWINGS FOR BUILDING LAYOUT AND DIMENSIONS AND PROPOSED SIGNS.



FORTY-FIGHT (48) HOURS FORTY-EIGHT (48) NOUNS BEFORE DIGGING IS TO COMMENCE, THE CONTRACTORS SHALL NOTIFY THE FOLLOWING AGENCIES: INDIANA UTLITIES PROTECTION SERVICE AT 811 OR 809-382-584 AND ALL OTHER AGENCIES WHICH MIGHT HAVE UNDERGROUND UTILITIES INVOLVING THIS PROJECT AND ARE NONMEMBERS OF STATE LITH ITIES PROTECTION SERVICE

VICINITY MAP

NO SCALE







FRANKLIN,

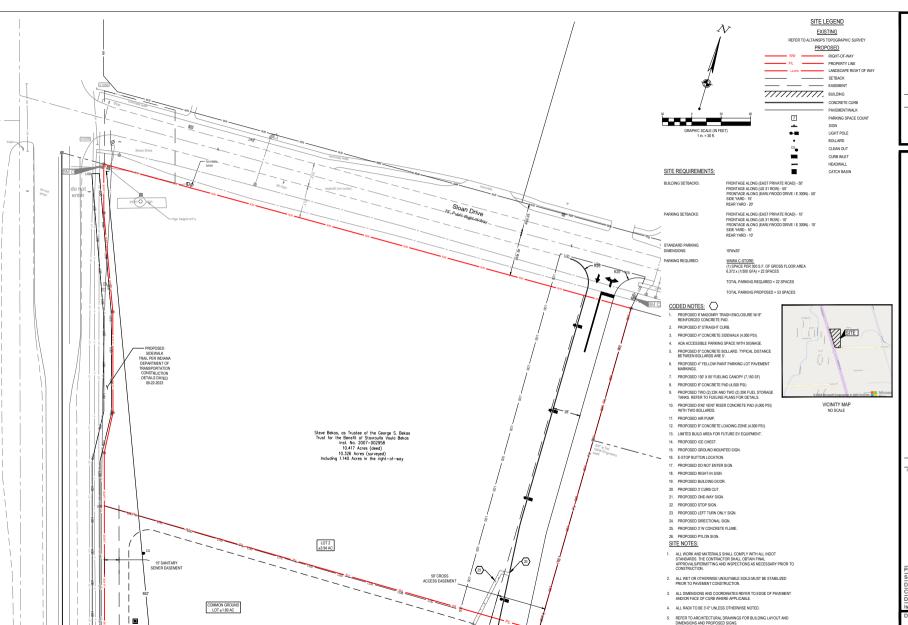
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12/04/2024

Issue: NOT FOR CONSTRUCTION Drawing Title SITE PLAN-SOUTH

Date:



(25)-

33' CROSS ACCESS EASEMENT

SEE SHEET 4 OF 15 SITE PLAN-SOUTH

WWW.execthe.com 7711 Bonhomme Ave., Suite 600 Clayton, MO 63105 Phone: 314.834.0063 Fax: 888.208.4621







FRANKLIN,

WAWA STORE #7426

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Project Number: 763219 1"=30" Drawn By: FAR Checked By: Date: 12/04/2024 Issue: NOT FOR CONSTRUCTION

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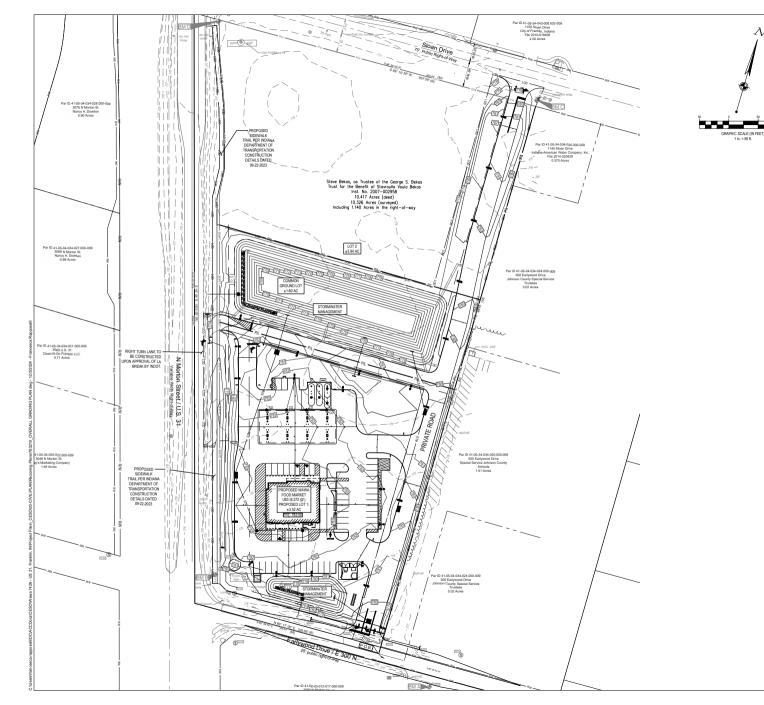
SITE PLAN-NORTH

5 OF 15

FOR 17-EIGHT (48) HOURS BEFORE DIGGING IS TO COMMENCE. THE CONTRACTORS SHALL NOTIFY THE FOLLOWING AGENCIES: INDIANA UTLITIES PROTECTION SERVICE AT 811 OR 800-382-584 AND ALL OTHER AGENCIES WHICH MIGHT HAVE UNDERGROUND UTILITIES Know what's below. Call before you dig. INVOLVING THIS PROJECT AND ARE NONMEMBERS OF STATE

FORTY-FIGHT (48) HOURS

UTILITIES PROTECTION SERVICE



GRADING LEGEND

EXISTING

REFER TO ALTAINSPS TOPOGRAPHIC SURVEY PROPOSED

PROPERTYLINE SETBACK MAJOR CONTOUR

////////, BUILDING 780 781

MINOR CONTOUR CDADE BREAK CLEAN OUT CURB INLET STORM SEWER LINE HEADWALL

GRADING NOTES:

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REFER TO SECTION 9 WAWA EARTHWORK / GRADING / CLEARING /
DEMOLITION SPECIFICATIONS FOR ADDITIONAL REQUIREMENTS THAT
SHOULD BE ACTORED IN BIOLORING PREPARAINE THE SITE. AND STRE
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CATCH BASIN







FRANKLIN,

WAWA STORE #7426

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Project Number: 763219 1" = 50" Drawn By: FAR Checked By: Date: 12/04/2024

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OVERALL GRADING

6 OF 15

FOR 17-EIGHT (48) HOURS BEFORE DIGGING IS TO COMMENCE. THE CONTRACTORS SHALL NOTIFY THE FOLLOWING AGENCIES: INDIANA UTLITIES PROTECTION SERVICE AT 811 OR 800-382-584 AND ALL OTHER AGENCIES WHICH MIGHT HAVE UNDERGROUND UTILITIES Know what's below. Call before you dig. INVOLVING THIS PROJECT AND ARE NONMEMBERS OF STATE

EARTHWORK QUANTITIES

*ESTIMATED QUANTITIES NOT FOR BIDDING

BM "B": Chiseled "X" southeast corner of concrete pad for signal pole. Northeast corner of U.S. 31 and Earlywood Dr., intersection, southwest from traffic control box. Elevation = 779.95"

BM "C": Chiseled "X" on arrow bolt west side of hydrant, south side of Sloan Rd., across the street from the fire station, near the end of the sidewalk. Elevation = 780.3 cm.

BM "D": Chiseled "X" on bolt west side of hydrant. West from telephone box southeast corner of Sloan Rd. and U.S. 31. Elevation = 778.03"

BENCHMARK Vertical Datum: NAVD88 derived from GPS Observations Benchnail set northwest corner of power pole. South side of Earlywood Dr., east from service entrance to Dodge

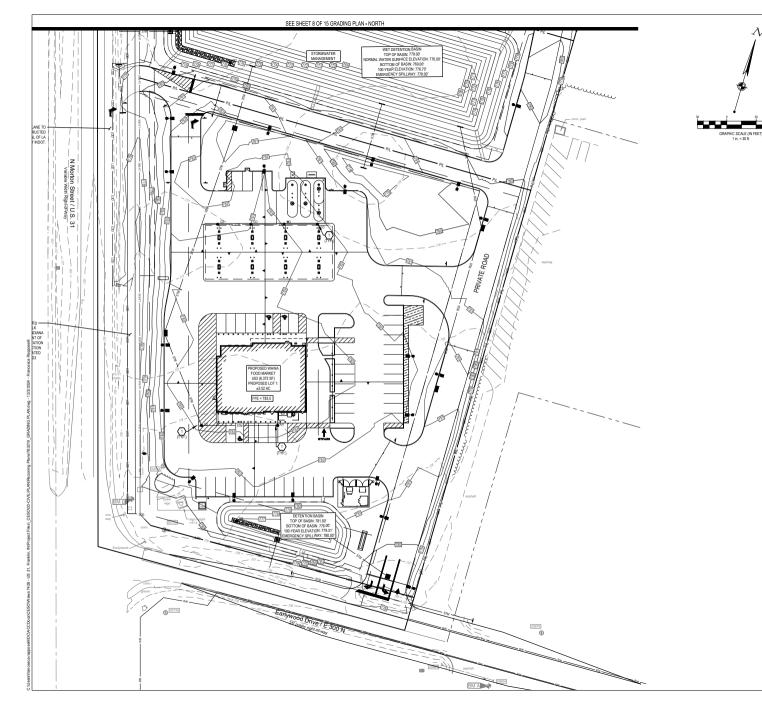
dealership. Elevation = 776.83'

RAW FILL (CY)

FORTY-FIGHT (48) HOURS

UTILITIES PROTECTION SERVICE

RAW CUT (CY)



GRADING LEGEND

EXISTING

REFER TO ALTAINSPS TOPOGRAPHIC SURVEY PROPOSED

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BUILDING

BUILDING

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STORM SEWER LINE
HEADWALL
CATCH BASIN
GRADING NOTES:

REFER TO SECTION 9 WWWA EARTHWORK / GRADING / CLEARING /
DEMOLITION SPECIFICATIONS FOR ADDITIONAL REQUIREMENTS THAT
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| EARTHWORK QUANTITIES | RAW CUT (CY) | RAW FILL (CY) | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055 | 20055

BENCHMARK
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Elevation = 778.63?
BM 'D': Chieseled "Y's outhwest corner of concrete pad for signal
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Elevation = 778.63?
BM 'C': Chieseled "X' on arrow boll west side only false.
BM 'C': Chieseled "X' on arrow boll west side of typicant, south
side of Sloss RRS, across the street from the fire festation,

BM "C": Chiseled "X" on arrow bolt west side of hydrant, south side of Sloan Rd., across the street from the fire station, near the end of the sidewalk.

Elevation = 780.33

BM "D": Chiseled "X" on bolt west side of hydrant. West from

BM "D": Chiseled "X" on bolt west side of hydrant. West from telephone box southeast corner of Sloan Rd. and U.S. 31. Elevation = 778.03"



FORTY-EIGHT (48) MOURS
BEFORE DIGGING IS TO
COMMENCE, THE CONTRACTORS
STALL NOTIFY THE FOLLOWING
AGENCIES INDIANA UTLITIES
PROTECTION SERVICE AT 81 TO
800-882-594 AND ALL OTHER
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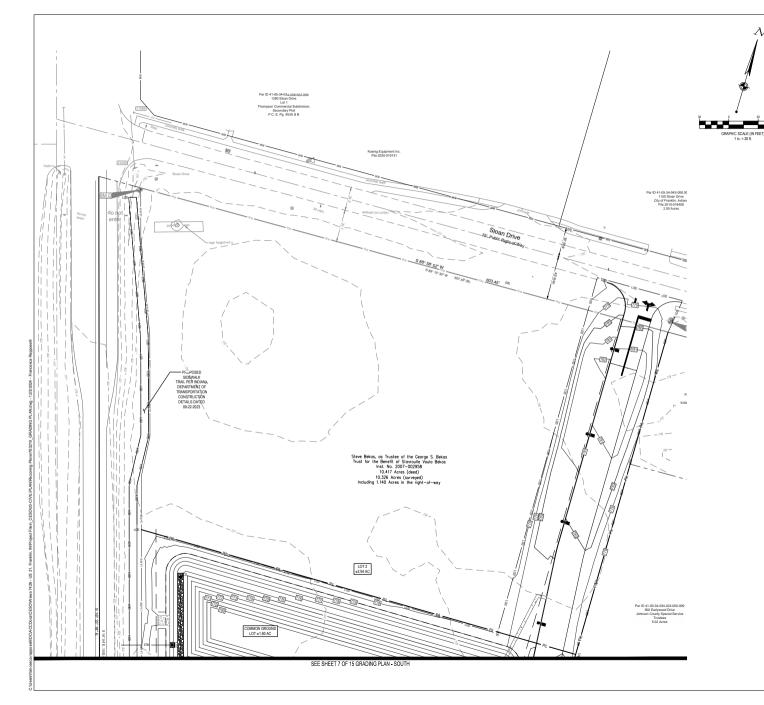
Revisions / Submissions

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| Project Number: 763219
| Scale: 1*=30'
| Drawn By: FAR
| Checked By: JTK
| Date: 12/04/2024
| Issue: NOT FOR CONSTRUCTION

Drawing Title:

GRADING PLAN -SOUTH



GRADING LEGEND

EXISTING

REFER TO ALTAINSPS TOPOGRAPHIC SURVEY PROPOSED

RIGHT-OF-WAY PROPERTY LINE - SETBACK ---- EASEMENT ////////, BUILDING MAJOR CONTOUR 780

781 MINOR CONTOUR GRADE BREAK CLEAN OUT CURR INLET HEADWALL



GRADING NOTES:

REFER TO SECTION 9 WAWA EARTHWORK / GRADING / CLEARING /
DEMOLITION SPECIFICATIONS FOR ADDITIONAL REQUIREMENTS THAT
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THE ENSMERT TO BETTAN CHARGHOLTON.

CODED NOTES:

1. WYE CONNECTION

EARTHWORK QUANTITIES RAW CUT (CY) RAW FILL (CY) *ESTIMATED QUANTITIES NOT FOR BIDDING

BENCHMARK Vertical Datum: NAVD88 derived from GPS Observations

Benchnail set northwest corner of power pole. South side of Earlywood Dr., east from service entrance to Dodge dealership. Elevation = 776.83'

BM 'B': Chickeled 'X' southeast corner of concrete pad for signal pole. Northeast corner of U.S. 31 and Earlywood Dr., intersection, southwest from traffic control box. Elevation = 779.95

BM "C": Chiseled "X" on arrow bolt west side of hydrant, south side of Sloan Rd., across the street from the fire station, near the end of the sidewalk. Elevation = 780.3 cm.

BM "D": Chiseled "X" on bolt west side of hydrant. West from telephone box southeast corner of Sloan Rd. and U.S. 31. Elevation = 778.03"



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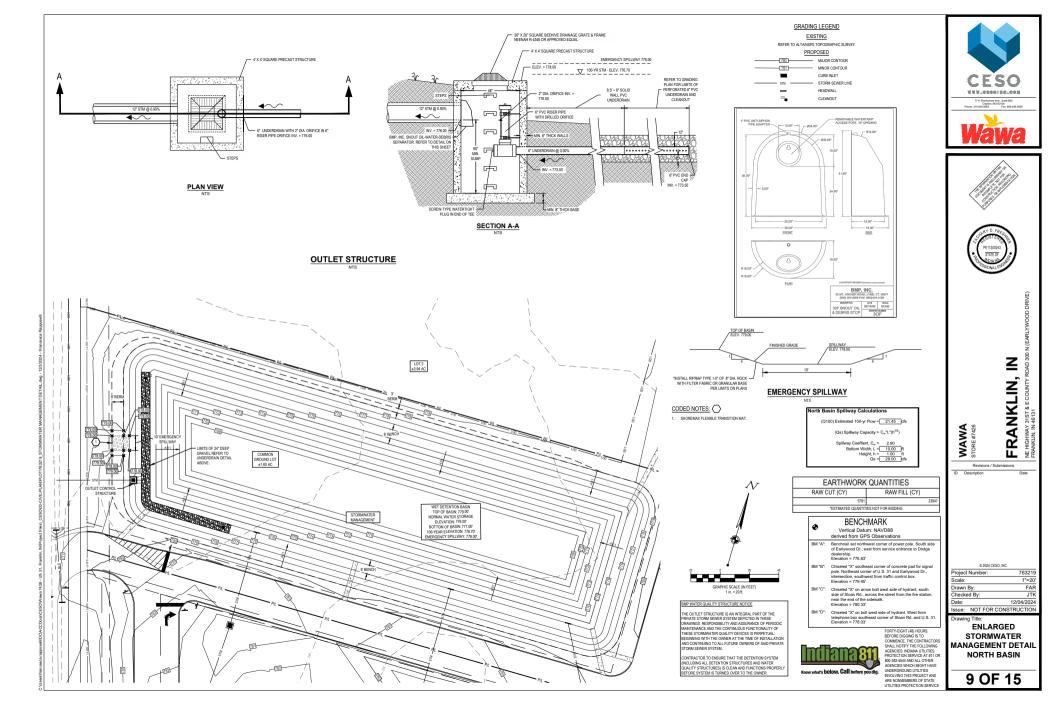
WAWA STORE #7426

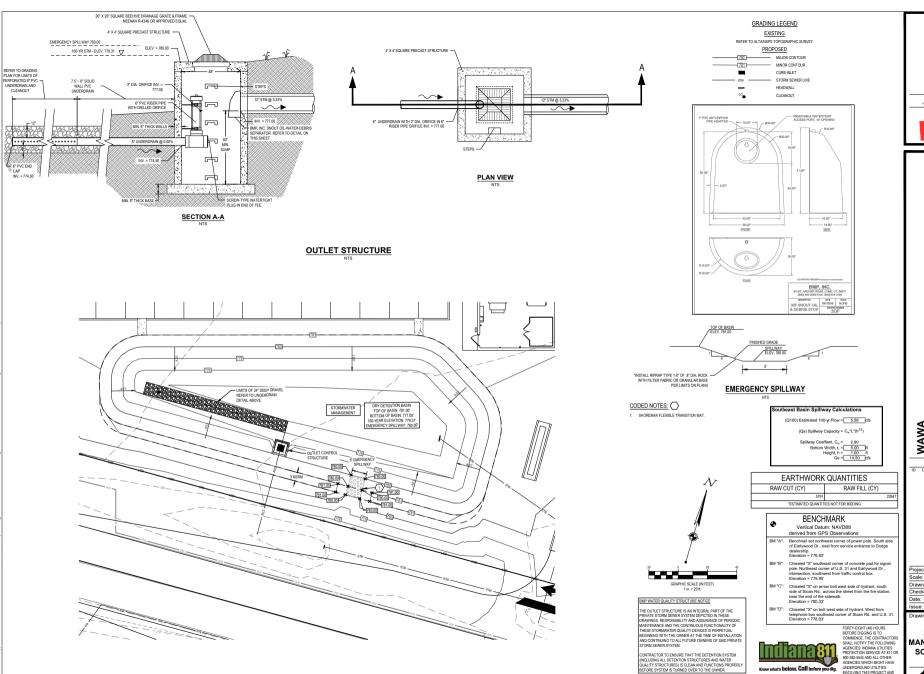
@ 2024 CESO, INC Project Number: 763219

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Drawing Title:

GRADING PLAN -NORTH













FRANKLIN,

WAWA STORE #7426

Project Number: 763219 Drawn By: FAR Checked By 12/04/2024 Issue: NOT FOR CONSTRUCTION

ENLARGED STORMWATER MANAGEMENT DETAIL SOUTHEAST BASIN

Know what's below. Call before you dig.

INVOLVING THIS PROJECT AND ARE NONMEMBERS OF STATE



APPENDIX B: PRE- AND POST-DEVELOPED DRAINAGE PLANS



FORTY-EIGHT (48) HOURS BEFORE DIOGNIG ST TO COMMENCE. THE CONTRACTORS SHALL NOTEY THE FOLLOWING AGENICES INDIANA UTILITIES PROTECTION SERVICE AT 811 OR 800-382-554 AND ALL OTHER AGENICES WHICH MIGHT HAVE UNDERGROUND UTILITIES INVOLVING THIS PROJECT AND ARE NONAMEMBERS OF STATE UTILITIES PROTECTION SERVICE





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WAWA STORE #7426

Project Number: 763219

1"=50" FAR JTK Drawn By: Checked By: Date: 09/05/2024 Issue: NOT FOR CONSTRUCTION

Drawing Title:

PRE-DEVELOPED DRAINAGE EXHIBIT

EX 1.0











FRANKLIN, IN

Revisions / Submissions

| D | Description | Date |

Drawing Title:

POST DEVELOPED DRAINAGE EXHIBIT

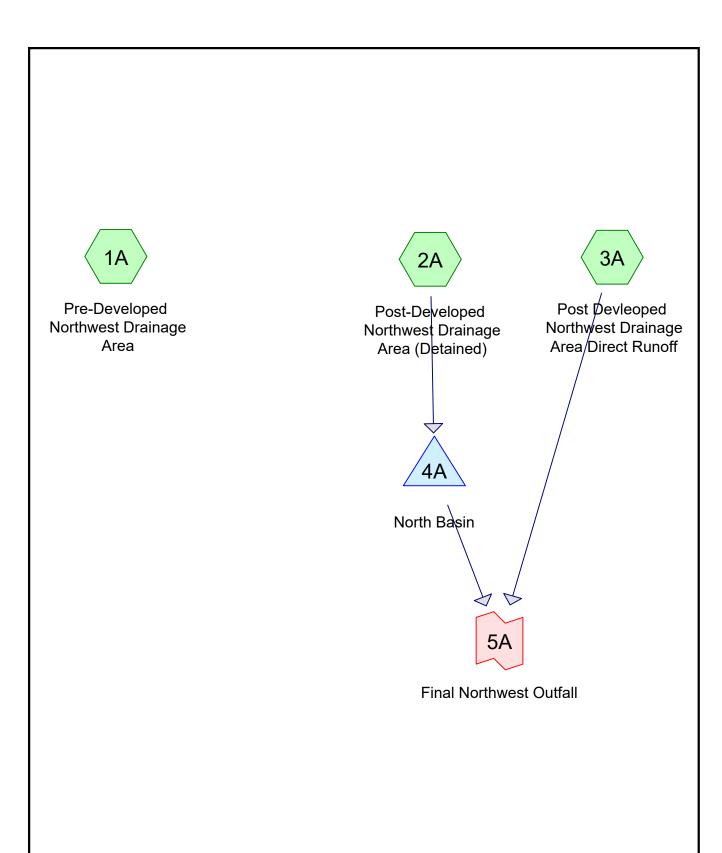
EX 2.0



APPENDIX C: HYDROCAD REPORT



APPENDIX C1.1: NORTHWEST DRAINAGE AREA REPORT











Wawa Franklin IN_HydroCAD Model (Northwest Drainage Area)

Prepared by CESO, Inc HydroCAD® 10.20-5c s/n 11958 © 2023 HydroCAD Software Solutions LLC

Printed 12/2/2024

Page 2

Rainfall Events Listing

Event#	Event	Storm Type	Curve	Mode	Duration	B/B	Depth	AMC
	Name				(hours)		(inches)	
1	2-YEAR	Huff 0-10sm	1Q	Scale	0.50	1	1.08	2
2	10-YEAR	Huff 0-10sm	1Q	Scale	0.50	1	1.57	2
3	100-YEAR	Huff 0-10sm	1Q	Scale	0.50	1	2.53	2

Page 3

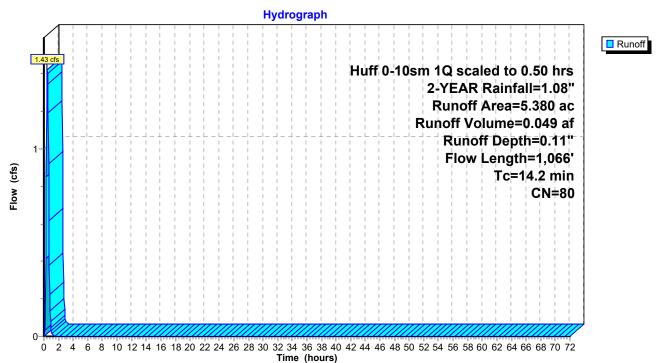
Summary for Subcatchment 1A: Pre-Developed Northwest Drainage Area

Runoff = 1.43 cfs @ 0.45 hrs, Volume= 0.049 af, Depth= 0.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 2-YEAR Rainfall=1.08"

 Area	(ac) C	N Des	cription		
5.	380 8	30 >75	% Grass co	over, Good	, HSG D
 5.	380	100	.00% Pervi	ous Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
 11.0	100	0.0170	0.15		Sheet Flow, Sheet Flow
3.2	343	0.0670	1.81		Grass: Short n= 0.150 P2= 2.91" Shallow Concentrated Flow, Shallow Concentrated Flow Short Grass Pasture Kv= 7.0 fps
0.0	623	0.2300	2,36219943	04,766.71	Channel Flow, Channel Flow
					Area= 4,361.0 sf Perim= 7.0' r= 623.00'
					n= 0.022 Earth, clean & straight
14.2	1,066	Total			

Subcatchment 1A: Pre-Developed Northwest Drainage Area



Wawa Franklin IN_HydroCAD Mode*Huff 0-10sm 1Q scaled to 0.50 hrs 2-YEAR Rainfall=1.08*" Prepared by CESO, Inc

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Summary for Subcatchment 2A: Post-Developed Northwest Drainage Area (Detained)

Runoff = 5.48 cfs @ 0.27 hrs, Volume= 0.151 af, Depth= 0.46"

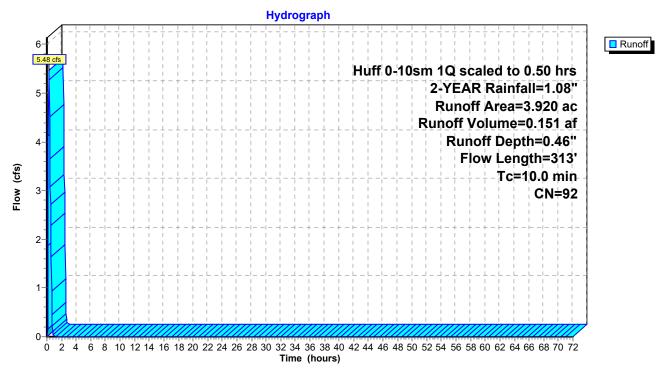
Routed to Pond 4A: North Basin

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 2-YEAR Rainfall=1.08"

Area	(ac) C	N Des	cription		
1	.330	80 >75	% Grass c	over, Good	, HSG D
2	2.590	98 Pav	ed parking	, HSG D	
3	3.920		ghted Aver		
	.330		3% Pervio		
2	2.590	66.0	7% Imper	∕ious Area	
т.	1 41-	Clara.	\	0:	Description
Tc (min)		•	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
2.9	100	0.0025	0.57		Sheet Flow, Sheet Flow
	4.0		4.00		Smooth surfaces n= 0.011 P2= 2.91"
0.7	43	0.0025	1.02		Shallow Concentrated Flow, Shallow Concentrated Flow
0.5	444	0.0004	0.74		Paved Kv= 20.3 fps
2.5	111	0.0021	0.74		Shallow Concentrated Flow, Shallow Concentrated Flow
0.6	24	0.0024	0.02		Unpaved Kv= 16.1 fps
0.6	34	0.0021	0.93		Shallow Concentrated Flow, Shallow Concentrated Flow
0.1	25	0.0330	2.92		Paved Kv= 20.3 fps Shallow Concentrated Flow, Shallow Concentrated Flow
0.1	25	0.0330	2.92		Unpaved Kv= 16.1 fps
3.2					Direct Entry, Direct Entry (To Reach Minmimum TOC)
		Total			Direct Litty, Direct Litty (10 Reach Milliann 100)
10.0	313	Total			

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Subcatchment 2A: Post-Developed Northwest Drainage Area (Detained)



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Summary for Subcatchment 3A: Post Devleoped Northwest Drainage Area Direct Runoff

Runoff = 0.55 cfs @ 0.37 hrs, Volume= 0.018 af, Depth= 0.19"

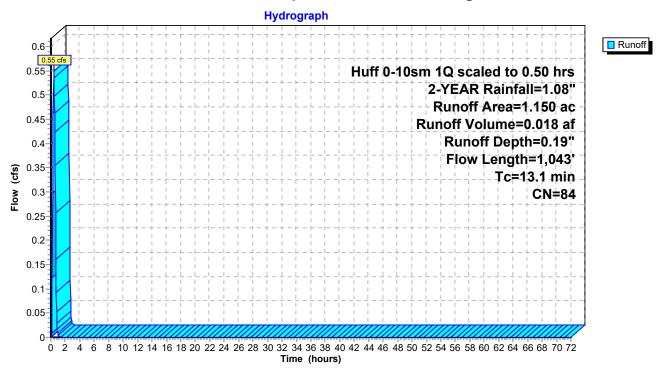
Routed to Link 5A: Final Northwest Outfall

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 2-YEAR Rainfall=1.08"

_	Area	(ac) C	N Des	cription		
	0.	880 8	30 >75	% Grass c	over, Good	, HSG D
	0.	270 9	98 Pave	ed parking	, HSG D	
	1.	150 8	34 Wei	ghted Aver	age	
	0.	880	76.5	2% Pervio	us Area	
	0.	270	23.4	8% Imper	vious Area	
	Τ.	1	01	V/-126	0	Description
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	12.6	100	0.0120	0.13		Sheet Flow, Sheet Flow
						Grass: Short n= 0.150 P2= 2.91"
	0.5	50	0.0110	1.69		Shallow Concentrated Flow, Shallow Concentrated Flow
						Unpaved Kv= 16.1 fps
	0.0	893	0.0150	767. 114 7	95,407.99	Channel Flow, Channel Flow
						Area= 6,251.0 sf Perim= 7.0' r= 893.00'
_						n= 0.022 Earth, clean & straight
	40.4	4 0 4 0	T-4-1			

13.1 1,043 Total

Subcatchment 3A: Post Devleoped Northwest Drainage Area Direct Runoff



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Summary for Pond 4A: North Basin

Inflow Area = 3.920 ac, 66.07% Impervious, Inflow Depth = 0.46" for 2-YEAR event

Inflow = 5.48 cfs @ 0.27 hrs, Volume= 0.151 af

Outflow = 0.05 cfs @ 0.86 hrs, Volume= 0.109 af, Atten= 99%, Lag= 35.0 min

Primary = 0.05 cfs @ 0.86 hrs, Volume= 0.109 af

Routed to Link 5A: Final Northwest Outfall

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 776.19' @ 0.86 hrs Surf.Area= 34,260 sf Storage= 6,492 cf

Plug-Flow detention time= 1,398.5 min calculated for 0.109 af (72% of inflow)

Center-of-Mass det. time= 1,394.1 min (1,416.0 - 21.8)

Volume	Inve	ert Avail.Sto	rage Storage	Description				
#1	776.0	00' 116,83	36 cf Custom	Stage Data (Pr	rismatic)Listed below (Recalc)			
Elevation (fee	et)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)				
776.0	-	33,587	0	0				
777.0	00	37,103	35,345	35,345				
778.0	00	40,720	38,912	74,257				
779.0	00	44,438	42,579	116,836				
Device	Routing	Invert	Outlet Device	S				
#1	Primary	776.00'	12.0" Round	Culvert L= 52.	.0' Ke= 0.500			
			n= 0.012 Cor	Inlet / Outlet Invert= 776.00' / 775.52' S= 0.0092 '/' Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 0.79 sf				
#2	Device 1	776.00'		2.5" Vert. Orifice/Grate (WQ Orifice) C= 0.600 Limited to weir flow at low heads				

778.00' 2.0" x 4.0" Horiz. Orifice/Grate X 6.00 columns

Limited to weir flow at low heads

X 5 rows C= 0.600 in 24.0" x 24.0" Grate (42% open area)

Primary OutFlow Max=0.05 cfs @ 0.86 hrs HW=776.19' (Free Discharge)

1=Culvert (Passes 0.05 cfs of 0.15 cfs potential flow)

—2=Orifice/Grate (WQ Orifice) (Orifice Controls 0.05 cfs @ 1.49 fps)

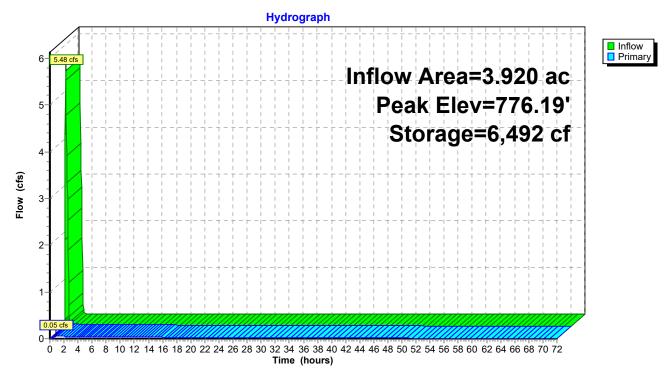
-3=Orifice/Grate (Controls 0.00 cfs)

#3

Device 1

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Pond 4A: North Basin



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Summary for Link 5A: Final Northwest Outfall

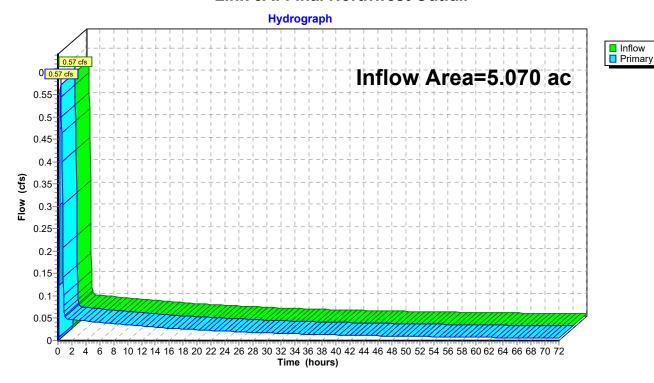
Inflow Area = 5.070 ac, 56.41% Impervious, Inflow Depth > 0.30" for 2-YEAR event

Inflow = 0.57 cfs @ 0.37 hrs, Volume= 0.127 af

Primary = 0.57 cfs @ 0.37 hrs, Volume= 0.127 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 5A: Final Northwest Outfall



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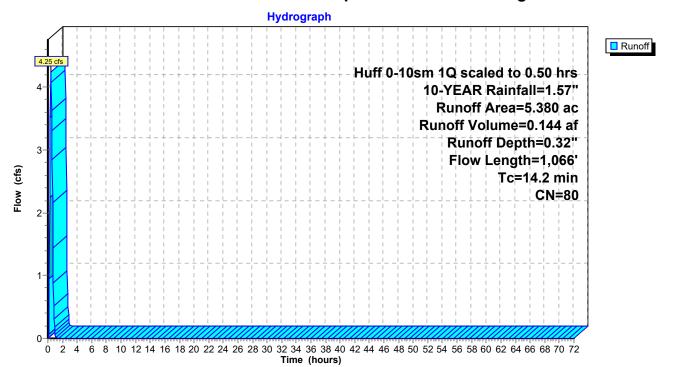
Summary for Subcatchment 1A: Pre-Developed Northwest Drainage Area

Runoff = 4.25 cfs @ 0.38 hrs, Volume= 0.144 af, Depth= 0.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 10-YEAR Rainfall=1.57"

 Area	(ac) C	N Des	cription		
5.	380 8	30 >75	% Grass co	over, Good	, HSG D
 5.	380	100	.00% Pervi	ous Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
 11.0	100	0.0170	0.15		Sheet Flow, Sheet Flow
3.2	343	0.0670	1.81		Grass: Short n= 0.150 P2= 2.91" Shallow Concentrated Flow, Shallow Concentrated Flow Short Grass Pasture Kv= 7.0 fps
0.0	623	0.2300	2,36219943	04,766.71	Channel Flow, Channel Flow
					Area= 4,361.0 sf Perim= 7.0' r= 623.00'
					n= 0.022 Earth, clean & straight
14.2	1,066	Total			

Subcatchment 1A: Pre-Developed Northwest Drainage Area



Wawa Franklin IN_HydroCAD Mod*Huff 0-10sm 1Q scaled to 0.50 hrs 10-YEAR Rainfall=1.57*" Prepared by CESO, Inc Printed 12/2/2024

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Summary for Subcatchment 2A: Post-Developed Northwest Drainage Area (Detained)

Runoff = 10.46 cfs @ 0.26 hrs, Volume= 0.281 af, Depth= 0.86"

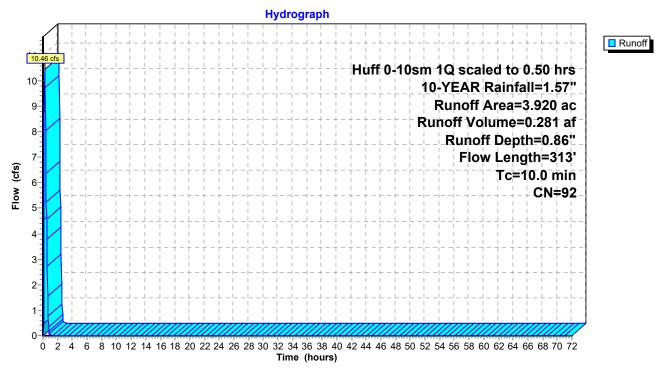
Routed to Pond 4A: North Basin

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 10-YEAR Rainfall=1.57"

Area	(ac) C	N Des	cription		
1	.330	80 >75	% Grass c	over, Good	, HSG D
2	2.590	98 Pav	ed parking	, HSG D	
3	3.920		ghted Aver		
	.330		3% Pervio		
2	2.590	66.0	7% Imper	∕ious Area	
т.	1 41-	Clara.	\	0:	Description
Tc (min)		•	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
2.9	100	0.0025	0.57		Sheet Flow, Sheet Flow
	4.0		4.00		Smooth surfaces n= 0.011 P2= 2.91"
0.7	43	0.0025	1.02		Shallow Concentrated Flow, Shallow Concentrated Flow
0.5	444	0.0004	0.74		Paved Kv= 20.3 fps
2.5	111	0.0021	0.74		Shallow Concentrated Flow, Shallow Concentrated Flow
0.6	24	0.0024	0.02		Unpaved Kv= 16.1 fps
0.6	34	0.0021	0.93		Shallow Concentrated Flow, Shallow Concentrated Flow
0.1	25	0.0330	2.92		Paved Kv= 20.3 fps Shallow Concentrated Flow, Shallow Concentrated Flow
0.1	25	0.0330	2.92		Unpaved Kv= 16.1 fps
3.2					Direct Entry, Direct Entry (To Reach Minmimum TOC)
		Total			Direct Litty, Direct Litty (10 Reach Milliann 100)
10.0	313	Total			

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Subcatchment 2A: Post-Developed Northwest Drainage Area (Detained)



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Summary for Subcatchment 3A: Post Devleoped Northwest Drainage Area Direct Runoff

Runoff = 1.37 cfs @ 0.34 hrs, Volume= 0.044 a

0.044 af, Depth= 0.46"

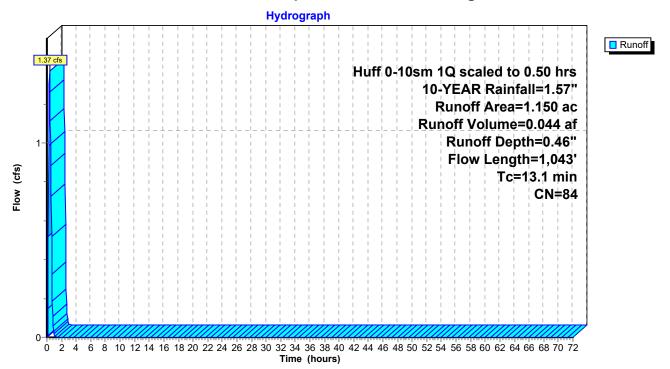
Routed to Link 5A: Final Northwest Outfall

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 10-YEAR Rainfall=1.57"

_	Area	(ac) C	N Des	cription		
0.880 80 >75% Grass cover, Good, H						, HSG D
	0.	270 9	98 Pave	ed parking	, HSG D	
	1.	150 8	34 Wei	ghted Aver	age	
	0.	880	76.5	2% Pervio	us Area	
	0.	270	23.4	8% Imper	vious Area	
	Tc	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	12.6	100	0.0120	0.13		Sheet Flow, Sheet Flow
						Grass: Short n= 0.150 P2= 2.91"
	0.5	50	0.0110	1.69		Shallow Concentrated Flow, Shallow Concentrated Flow
						Unpaved Kv= 16.1 fps
	0.0	893	0.0150	767. 114 7	95,407.99	Channel Flow, Channel Flow
						Area= 6,251.0 sf Perim= 7.0' r= 893.00'
_						n= 0.022 Earth, clean & straight
	12 1	1 0/12	Total			

13.1 1,043 Total

Subcatchment 3A: Post Devleoped Northwest Drainage Area Direct Runoff



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Summary for Pond 4A: North Basin

Inflow Area = 3.920 ac, 66.07% Impervious, Inflow Depth = 0.86" for 10-YEAR event

Inflow 10.46 cfs @ 0.26 hrs. Volume= 0.281 af

Outflow 0.08 cfs @ 0.85 hrs, Volume= 0.224 af, Atten= 99%, Lag= 35.6 min

Primary 0.08 cfs @ 0.85 hrs, Volume= 0.224 af

Routed to Link 5A: Final Northwest Outfall

Routing by Stor-Ind method. Time Span= 0.00-72.00 hrs. dt= 0.05 hrs. Peak Elev= 776.35' @ 0.85 hrs Surf.Area= 34,828 sf Storage= 12,075 cf

Plug-Flow detention time= 1,429.2 min calculated for 0.224 af (80% of inflow)

Center-of-Mass det. time= 1,425.8 min (1,446.8 - 21.0)

Volume	Inv	ert Avail.Sto	rage Storage	Description			
#1	776.0	00' 116,8	36 cf Custon	n Stage Data (P	rismatic)Listed below (Recalc)		
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)			
776.0		33,587	0	(Cubic-leet)			
777.0		37,103	35,345	35,345			
778.0	00	40,720	38,912	74,257			
779.0	00	44,438	42,579	116,836			
Device Routing		Invert	Outlet Device	es			
#1	Primary	776.00'	12.0" Round	d Culvert L= 52	.0' Ke= 0.500		
			Inlet / Outlet Invert= 776.00' / 775.52' S= 0.0092 '/' Cc= 0.900				
~		•	ooth interior, Flow Area= 0.79 sf				
#2	Device 1	776.00'	2.5" Vert. Orifice/Grate (WQ Orifice) C= 0.600				
		770 001	Limited to weir flow at low heads				
#3	Device 1	778.00'	2.0" x 4.0" Horiz. Orifice/Grate X 6.00 columns				
			X 5 rows C=	0.600 in 24.0" x	24.0" Grate (42% open area)		

Limited to weir flow at low heads

Primary OutFlow Max=0.08 cfs @ 0.85 hrs HW=776.35' (Free Discharge)

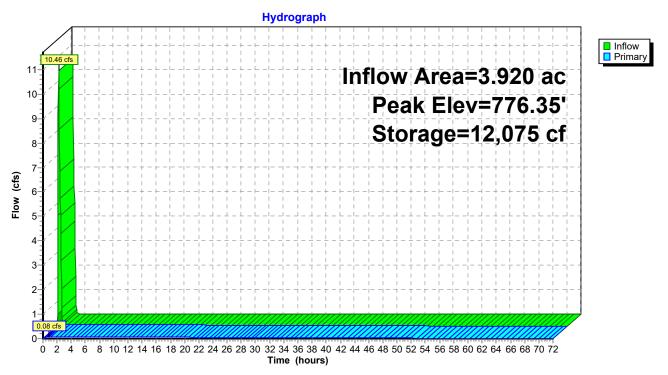
-1=Culvert (Passes 0.08 cfs of 0.49 cfs potential flow)

—2=Orifice/Grate (WQ Orifice) (Orifice Controls 0.08 cfs @ 2.40 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

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Pond 4A: North Basin



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Summary for Link 5A: Final Northwest Outfall

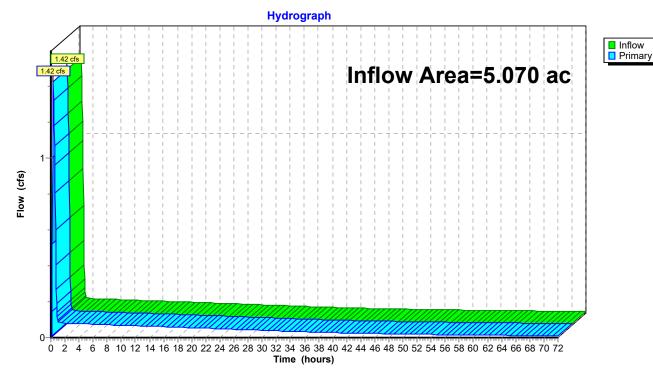
Inflow Area = 5.070 ac, 56.41% Impervious, Inflow Depth > 0.63" for 10-YEAR event

Inflow = 1.42 cfs @ 0.35 hrs, Volume= 0.268 af

Primary = 1.42 cfs @ 0.35 hrs, Volume= 0.268 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 5A: Final Northwest Outfall



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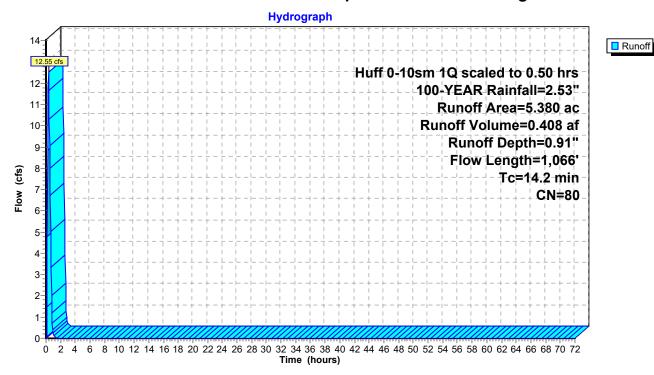
Summary for Subcatchment 1A: Pre-Developed Northwest Drainage Area

Runoff = 12.55 cfs @ 0.35 hrs, Volume= 0.408 af, Depth= 0.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 100-YEAR Rainfall=2.53"

	Area	(ac) C	N Des	cription		
5.380 80 >75% Grass cover, Good,					over, Good	, HSG D
5.380 100.00% Pervious Area						
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	11.0	100	0.0170	0.15		Sheet Flow, Sheet Flow
	3.2	343	0.0670	1.81		Grass: Short n= 0.150 P2= 2.91" Shallow Concentrated Flow, Shallow Concentrated Flow Short Grass Pasture Kv= 7.0 fps
	0.0	623	0.2300	2,3621994304,766.71		Channel Flow, Channel Flow Area= 4,361.0 sf Perim= 7.0' r= 623.00' n= 0.022 Earth, clean & straight
	14 2	1 066	Total		•	

Subcatchment 1A: Pre-Developed Northwest Drainage Area



Wawa Franklin IN_HydroCAD Mo*Huff 0-10sm 1Q scaled to 0.50 hrs 100-YEAR Rainfall=2.53"*Prepared by CESO, Inc Printed 12/2/2024

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Summary for Subcatchment 2A: Post-Developed Northwest Drainage Area (Detained)

Runoff = 21.45 cfs @ 0.25 hrs, Volume= 0.562 af, Depth= 1.72"

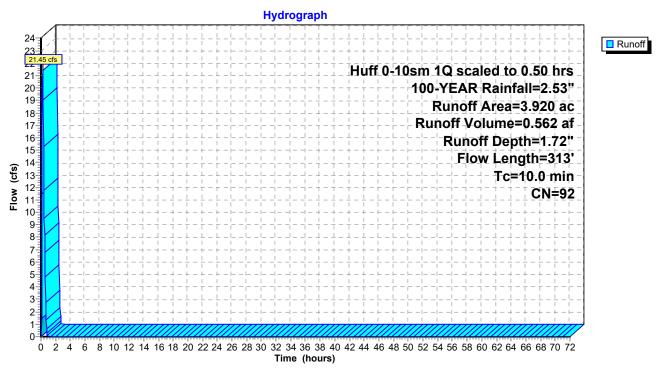
Routed to Pond 4A: North Basin

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 100-YEAR Rainfall=2.53"

Area	(ac) C	N Des	cription		
1	.330	80 >75	% Grass c	over, Good	, HSG D
2	2.590	98 Pav	ed parking	, HSG D	
3	3.920		ghted Aver		
	.330		3% Pervio		
2	2.590	66.0	7% Imper	∕ious Area	
т.	1 41-	Clara.	\	0:	Description
Tc (min)		•	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
2.9	100	0.0025	0.57		Sheet Flow, Sheet Flow
	4.0		4.00		Smooth surfaces n= 0.011 P2= 2.91"
0.7	43	0.0025	1.02		Shallow Concentrated Flow, Shallow Concentrated Flow
0.5	444	0.0004	0.74		Paved Kv= 20.3 fps
2.5	111	0.0021	0.74		Shallow Concentrated Flow, Shallow Concentrated Flow
0.6	24	0.0024	0.02		Unpaved Kv= 16.1 fps
0.6	34	0.0021	0.93		Shallow Concentrated Flow, Shallow Concentrated Flow
0.1	25	0.0330	2.92		Paved Kv= 20.3 fps Shallow Concentrated Flow, Shallow Concentrated Flow
0.1	25	0.0330	2.92		Unpaved Kv= 16.1 fps
3.2					Direct Entry, Direct Entry (To Reach Minmimum TOC)
		Total			Direct Litty, Direct Litty (10 Reach Milliann 100)
10.0	313	Total			

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Subcatchment 2A: Post-Developed Northwest Drainage Area (Detained)



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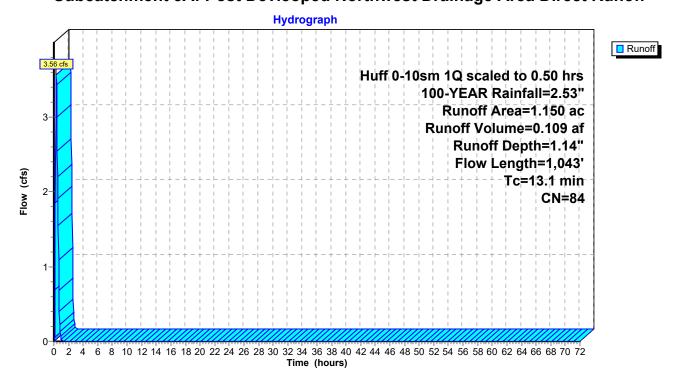
Summary for Subcatchment 3A: Post Devleoped Northwest Drainage Area Direct Runoff

Runoff = 3.56 cfs @ 0.32 hrs, Volume= 0.109 af, Depth= 1.14" Routed to Link 5A : Final Northwest Outfall

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 100-YEAR Rainfall=2.53"

Area (ac) CN Desc		cription				
	0.8	880 8	30 >75°	% Grass c	over, Good	, HSG D
	0.2	270 9	8 Pave	ed parking	, HSG D	
	1.	150 8	34 Weig	ghted Aver	age	
	0.8	880	76.5	2% Pervio	us Area	
	0.2	270	23.4	8% Imper	∕ious Area	
	_				_	
	Tc	Length	Slope	Velocity	Capacity	Description
(n	nin)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
1	12.6	100	0.0120	0.13		Sheet Flow, Sheet Flow
						Grass: Short n= 0.150 P2= 2.91"
	0.5	50	0.0110	1.69		Shallow Concentrated Flow, Shallow Concentrated Flow
						Unpaved Kv= 16.1 fps
	0.0	893	0.0150	767. 114 7	95,407.99	Channel Flow, Channel Flow
						Area= 6,251.0 sf Perim= 7.0' r= 893.00'
						n= 0.022 Earth, clean & straight
1	13.1	1,043	Total			

Subcatchment 3A: Post Devleoped Northwest Drainage Area Direct Runoff



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Summary for Pond 4A: North Basin

Inflow Area = 3.920 ac, 66.07% Impervious, Inflow Depth = 1.72" for 100-YEAR event

Inflow = 21.45 cfs @ 0.25 hrs, Volume= 0.562 af

Outflow = 0.13 cfs @ 0.86 hrs, Volume= 0.460 af, Atten= 99%, Lag= 36.9 min

Primary = 0.13 cfs @ 0.86 hrs, Volume= 0.460 af

Routed to Link 5A: Final Northwest Outfall

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 776.70' @ 0.86 hrs Surf.Area= 36,032 sf Storage= 24,208 cf

Plug-Flow detention time= 1,688.4 min calculated for 0.459 af (82% of inflow)

Center-of-Mass det. time= 1,687.0 min (1,707.1 - 20.1)

Volume	Inve	rt Avail.Sto	rage Storage	e Description				
#1	776.0	0' 116,83	36 cf Custon	cf Custom Stage Data (Prismatic)Listed below (Recalc)				
Elevation (feet)		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)				
776.00		33,587	0	0				
777.0	00	37,103	35,345	35,345				
778.0	00	40,720	38,912	74,257				
779.0	00	44,438	42,579	116,836				
Device	Routing	Invert	Outlet Device	es				
#1	Primary	776.00'	12.0" Round	d Culvert L= 52	.0' Ke= 0.500			
	•		Inlet / Outlet Invert= 776.00' / 775.52' S= 0.0092 '/' Cc= 0.900					
			n= 0.012 Co	rrugated PP, sm	ooth interior, Flow Area= 0.79 sf			
#2	Device 1	776.00'	2.5" Vert. Or	rifice/Grate (WQ	Orifice) C= 0.600			
			Limited to we	eir flow at low hea	ads			
#3	Device 1	778.00'			ate X 6.00 columns			
			X 5 rows C= 0.600 in 24.0" x 24.0" Grate (42% open area)					

Limited to weir flow at low heads

Primary OutFlow Max=0.13 cfs @ 0.86 hrs HW=776.70' (Free Discharge)

1=Culvert (Passes 0.13 cfs of 1.59 cfs potential flow)

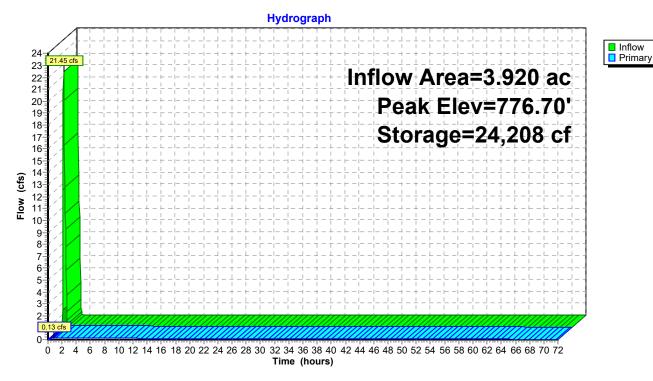
—2=Orifice/Grate (WQ Orifice) (Orifice Controls 0.13 cfs @ 3.70 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

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Pond 4A: North Basin



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Summary for Link 5A: Final Northwest Outfall

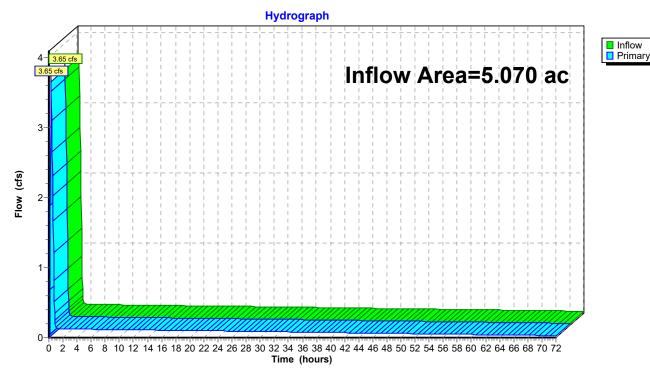
Inflow Area = 5.070 ac, 56.41% Impervious, Inflow Depth > 1.35" for 100-YEAR event

Inflow = 3.65 cfs @ 0.32 hrs, Volume= 0.569 af

Primary = 3.65 cfs @ 0.32 hrs, Volume= 0.569 af, Atten= 0%, Lag= 0.0 min

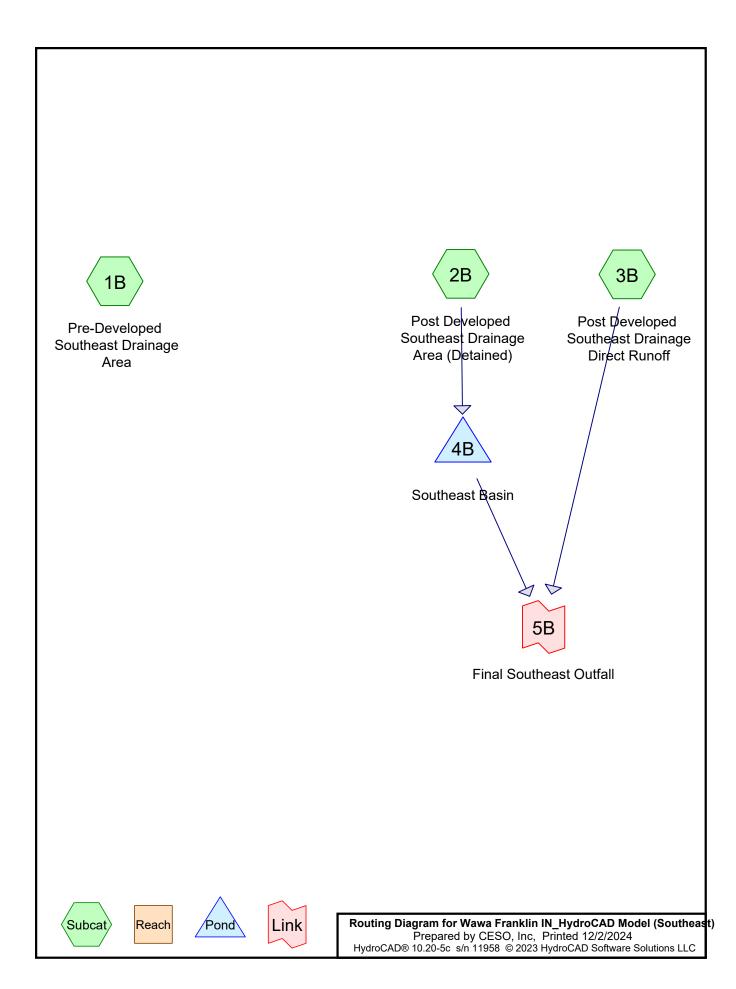
Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 5A: Final Northwest Outfall





APPENDIX C1.2: SOUTHEAST DRAINAGE AREA REPORT



Wawa Franklin IN_HydroCAD Model (Southeast) Prepared by CESO, Inc HydroCAD® 10.20-5c s/n 11958 © 2023 HydroCAD Software Solutions LLC

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Rainfall Events Listing

Event#	Event	Storm Type	Curve	Mode	Duration	B/B	Depth	AMC
	Name				(hours)		(inches)	
1	2-YEAR	Huff 0-10sm	1Q	Scale	0.50	1	1.08	2
2	10-YEAR	Huff 0-10sm	1Q	Scale	0.50	1	1.57	2
3	100-YEAR	Huff 0-10sm	1Q	Scale	0.50	1	2.53	2

Page 3

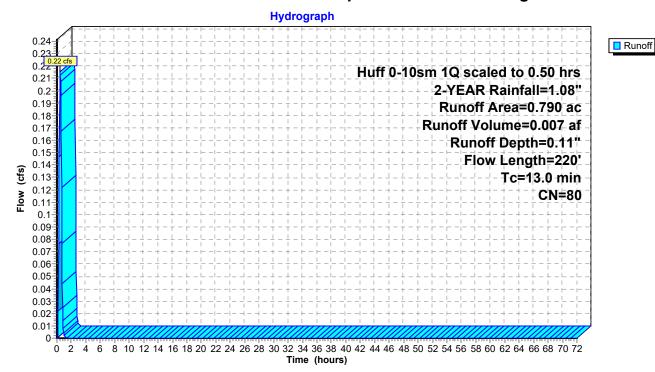
Summary for Subcatchment 1B: Pre-Developed Southeast Drainage Area

Runoff = 0.22 cfs @ 0.42 hrs, Volume= 0.007 af, Depth= 0.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 2-YEAR Rainfall=1.08"

_	Area	(ac) C	N Des	cription		
_	0.	790 8	30 >75°	% Grass c	over, Good	, HSG D
0.790 100.00% Pervious Area						
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	11.2	100	0.0160	0.15	, ,	Sheet Flow, Sheet Flow
	1.8	120	0.0240	1.08		Grass: Short n= 0.150 P2= 2.91" Shallow Concentrated Flow, Shallow Concentrated Flow Short Grass Pasture Kv= 7.0 fps
_	13.0	220	Total	•		

Subcatchment 1B: Pre-Developed Southeast Drainage Area



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Summary for Subcatchment 2B: Post Developed Southeast Drainage Area (Detained)

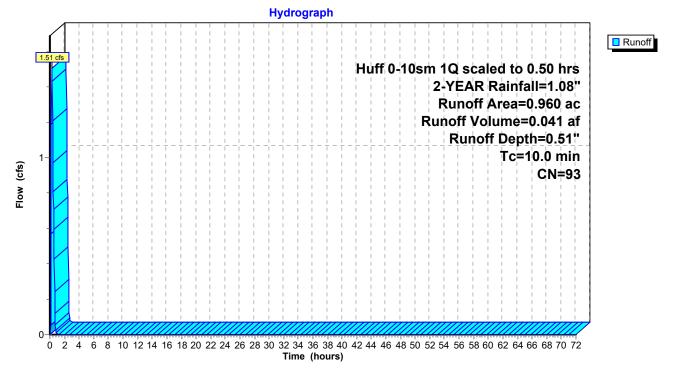
Runoff = 1.51 cfs @ 0.27 hrs, Volume= 0.041 af, Depth= 0.51"

Routed to Pond 4B: Southeast Basin

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 2-YEAR Rainfall=1.08"

	Area	(ac)	CN	Desc	Description							
	0.	260	80	>75%	√ Grass co	over, Good	, HSG D					
0.700 98 Paved parking, HSG D												
0.960 93 Weighted Average						age						
0.260 27.08% Pervious Area						us Area						
	0.700			72.92% Impervious Area								
	_		ci.	01	V/.1	0	December 1999					
,		Leng		Slope	Velocity	Capacity	Description					
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)						
	10.0						Direct Entry, Direct Entry					

Subcatchment 2B: Post Developed Southeast Drainage Area (Detained)



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Summary for Subcatchment 3B: Post Developed Southeast Drainage Direct Runoff

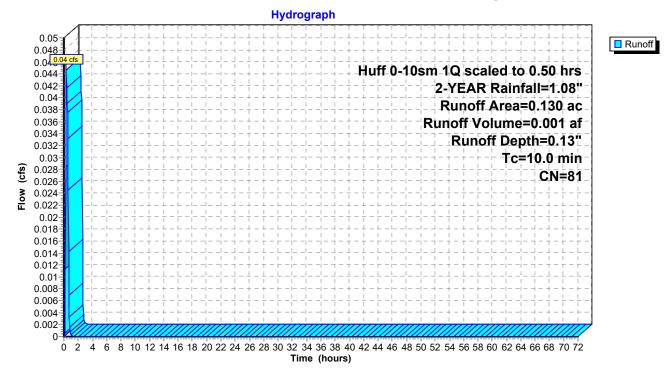
0.001 af, Depth= 0.13" Runoff 0.04 cfs @ 0.35 hrs, Volume= Routed to Link 5B: Final Southeast Outfall

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 2-YEAR Rainfall=1.08"

	Area	(ac)	CN	Desc	Description							
	0.	120	80	>75%	6 Grass co	over, Good	, HSG D					
	0.010 98 Paved parking, HSG D											
	0.	130	81	Weig	hted Aver	age						
	0.120 92.31% Pervious Area											
	0.010			7.69	7.69% Impervious Area							
	_			01		.						
	Tc	Leng		Slope	Velocity	Capacity	Description					
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)						
	10.0						Direct Entry, Direct Entry					

Direct Entry, Direct Entry

Subcatchment 3B: Post Developed Southeast Drainage Direct Runoff



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Summary for Pond 4B: Southeast Basin

Inflow Area = 0.960 ac, 72.92% Impervious, Inflow Depth = 0.51" for 2-YEAR event

Inflow = 1.51 cfs @ 0.27 hrs, Volume= 0.041 af

Outflow = 0.09 cfs @ 0.72 hrs, Volume= 0.041 af, Atten= 94%, Lag= 27.2 min

Primary = 0.09 cfs @ 0.72 hrs, Volume = 0.041 af

Routed to Link 5B: Final Southeast Outfall

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 777.87' @ 0.72 hrs Surf.Area= 2,270 sf Storage= 1,621 cf

Plug-Flow detention time= 218.8 min calculated for 0.041 af (100% of inflow)

Center-of-Mass det. time= 220.3 min (241.7 - 21.5)

Volume	Inv	ert Avail.Sto	rage Storage	e Description	
#1	777.0	00' 14,2	36 cf Custon	n Stage Data (P	rismatic)Listed below (Recalc)
Elevatio		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
777.0	00	1,441	0	0	
778.0	00	2,390	1,916	1,916	
779.0	00	3,477	2,934	4,849	
780.0	00	4,669	4,073	8,922	
781.0	00	5,959	5,314	14,236	
Device	Routing	Invert	Outlet Device	es	
#1	Primary	777.00'	12.0" Roun	d Culvert L= 30	.0' Ke= 0.500
	•		Inlet / Outlet	Invert= 777.00' /	776.00' S= 0.0333 '/' Cc= 0.900
			n= 0.012 Co	rrugated PP, sm	ooth interior, Flow Area= 0.79 sf
#2	Device 1	777.00'	2.0" Vert. Oi	rifice/Grate C=	0.600 Limited to weir flow at low heads
#3	Device 1	780.00'	2.0" x 4.0" H	loriz. Orifice/Gra	ate X 6.00 columns
			X 5 rows C=	0.600 in 24.0" x	24.0" Grate (42% open area)
			Limited to we	eir flow at low hea	ads

Primary OutFlow Max=0.09 cfs @ 0.72 hrs HW=777.87' (Free Discharge)

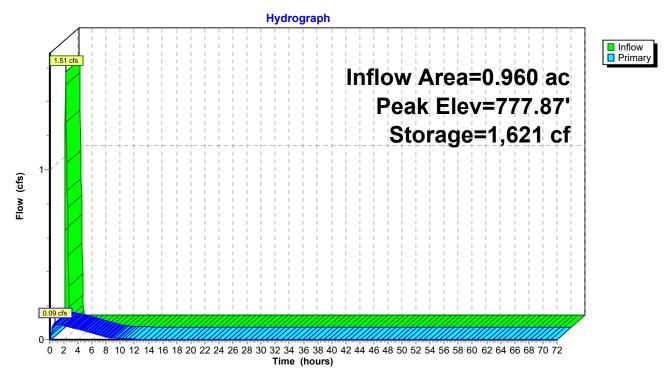
_1=Culvert (Passes 0.09 cfs of 2.31 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.09 cfs @ 4.28 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

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Pond 4B: Southeast Basin



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Summary for Link 5B: Final Southeast Outfall

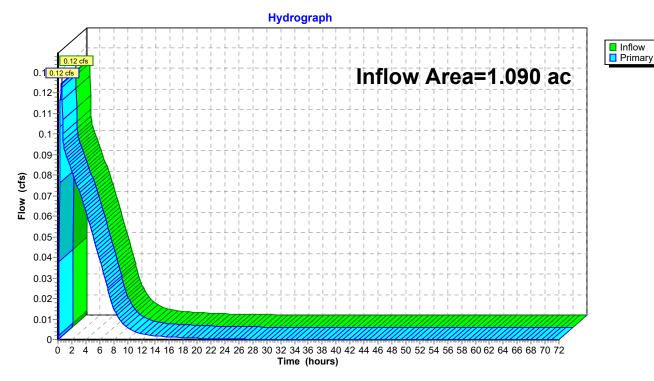
Inflow Area = 1.090 ac, 65.14% Impervious, Inflow Depth = 0.47" for 2-YEAR event

Inflow = 0.12 cfs @ 0.50 hrs, Volume= 0.042 af

Primary = 0.12 cfs @ 0.50 hrs, Volume= 0.042 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 5B: Final Southeast Outfall



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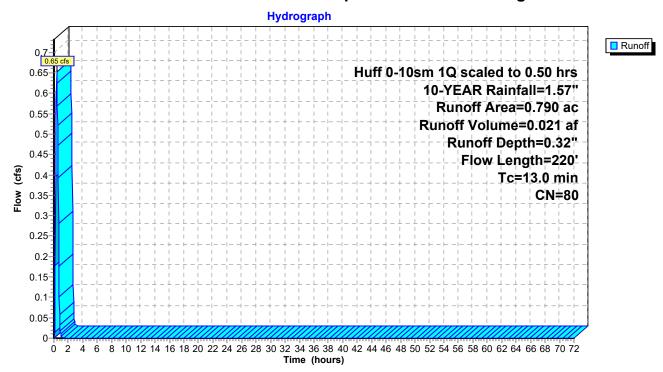
Summary for Subcatchment 1B: Pre-Developed Southeast Drainage Area

Runoff = 0.65 cfs @ 0.36 hrs, Volume= 0.021 af, Depth= 0.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 10-YEAR Rainfall=1.57"

	Area	(ac) C	N Des	cription		
	0.	790 8	30 >75°	% Grass c	over, Good	, HSG D
	0.	790	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	11.2	100	0.0160	0.15	,	Sheet Flow, Sheet Flow
	1.8	120	0.0240	1.08		Grass: Short n= 0.150 P2= 2.91" Shallow Concentrated Flow, Shallow Concentrated Flow Short Grass Pasture Kv= 7.0 fps
-	13.0	220	Total	·		

Subcatchment 1B: Pre-Developed Southeast Drainage Area



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Summary for Subcatchment 2B: Post Developed Southeast Drainage Area (Detained)

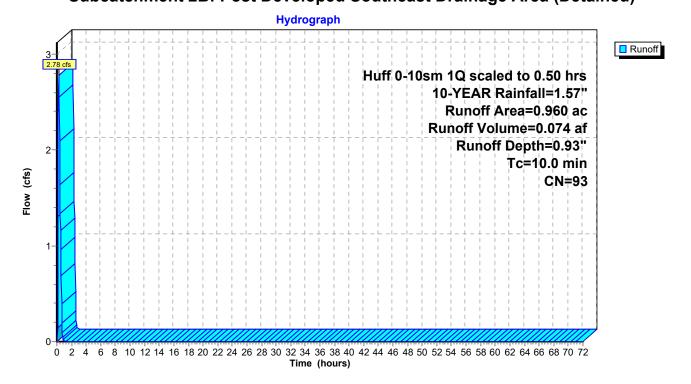
Runoff = 2.78 cfs @ 0.26 hrs, Volume= 0.074 af, Depth= 0.93"

Routed to Pond 4B: Southeast Basin

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 10-YEAR Rainfall=1.57"

	Area	(ac)	CN	Desc	Description							
	0.	260	80	>75%	√ Grass co	over, Good	, HSG D					
	0.700 98 Paved parking, HSG D											
0.960 93 Weighted Average					hted Aver	age						
	0.260 27.08% Pervious Area											
	0.700			72.92	2% Imperv	ious Area						
	Тс	Leng	th :	Slope	Velocity	Capacity	Description					
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)						
	10.0						Direct Entry, Direct Entry					

Subcatchment 2B: Post Developed Southeast Drainage Area (Detained)



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Summary for Subcatchment 3B: Post Developed Southeast Drainage Direct Runoff

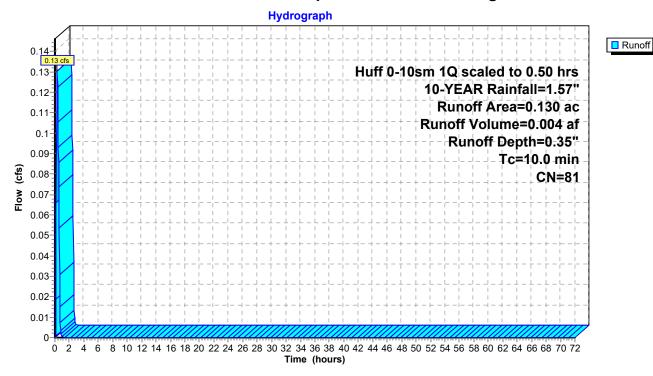
0.004 af, Depth= 0.35" Runoff 0.13 cfs @ 0.31 hrs, Volume= Routed to Link 5B: Final Southeast Outfall

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 10-YEAR Rainfall=1.57"

	Area	(ac)	CN	Desc	Description							
	0.	120	80	>75%	% Grass co	over, Good	, HSG D					
	0.	010	98	Pave	ed parking	, HSG D						
	0.130 81 Weighted Average											
	0.	120		92.3	1% Pervio	us Area						
	0.010 7.69% Impervious Area				% Impervi	ous Area						
	Тс	Leng	th	Slope	Velocity	Capacity	Description					
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)						
	10.0						Direct Entry, Direct Entry					

Direct Entry, Direct Entry

Subcatchment 3B: Post Developed Southeast Drainage Direct Runoff



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Summary for Pond 4B: Southeast Basin

Inflow Area = 0.960 ac, 72.92% Impervious, Inflow Depth = 0.93" for 10-YEAR event

Inflow = 2.78 cfs @ 0.26 hrs, Volume= 0.074 af

Outflow = 0.12 cfs @ 0.74 hrs, Volume= 0.074 af, Atten= 96%, Lag= 28.9 min

Primary = 0.12 cfs @ 0.74 hrs, Volume= 0.074 af

Routed to Link 5B: Final Southeast Outfall

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 778.41' @ 0.74 hrs Surf.Area= 2,839 sf Storage= 2,996 cf

Plug-Flow detention time= 283.1 min calculated for 0.074 af (100% of inflow)

Center-of-Mass det. time= 284.5 min (305.2 - 20.7)

Volume	Inv	ert Avail.Sto	rage Stora	age Description	
#1	777.	00' 14,2	36 cf Cust	tom Stage Data (P	rismatic)Listed below (Recalc)
Elevatio		Surf.Area (sq-ft)	Inc.Store	•	
777.0	00	1,441	C	0	
778.0	00	2,390	1,916	1,916	
779.0	00	3,477	2,934	4,849	
780.0	00	4,669	4,073	8,922	
781.0	00	5,959	5,314	14,236	
Device	Routing	Invert	Outlet Dev	vices	
#1	Primary	777.00'	12.0" Ro	und Culvert L= 30	.0' Ke= 0.500
	•		Inlet / Out	let Invert= 777.00' /	776.00' S= 0.0333 '/' Cc= 0.900
				9	ooth interior, Flow Area= 0.79 sf
#2	Device '	1 777.00'	2.0" Vert.	Orifice/Grate C=	0.600 Limited to weir flow at low heads
#3	Device '	1 780.00'	-		ate X 6.00 columns
					24.0" Grate (42% open area)
			Limited to	weir flow at low hea	ads

Primary OutFlow Max=0.12 cfs @ 0.74 hrs HW=778.41' (Free Discharge)

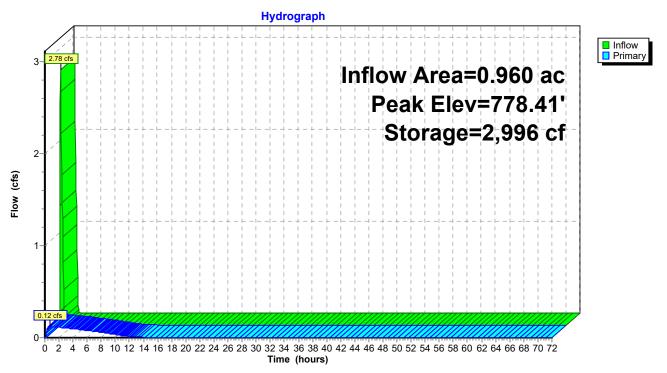
1=Culvert (Passes 0.12 cfs of 3.61 cfs potential flow)

—2=Orifice/Grate (Orifice Controls 0.12 cfs @ 5.55 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

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Pond 4B: Southeast Basin



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Primary

Summary for Link 5B: Final Southeast Outfall

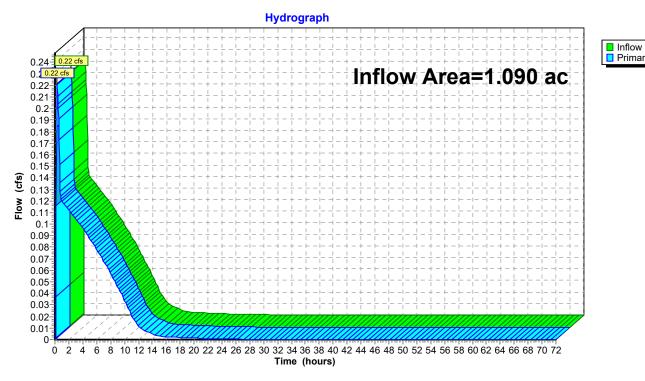
1.090 ac, 65.14% Impervious, Inflow Depth = 0.86" for 10-YEAR event Inflow Area =

0.34 hrs, Volume= Inflow 0.22 cfs @ 0.078 af

0.34 hrs, Volume= Primary 0.22 cfs @ 0.078 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 5B: Final Southeast Outfall



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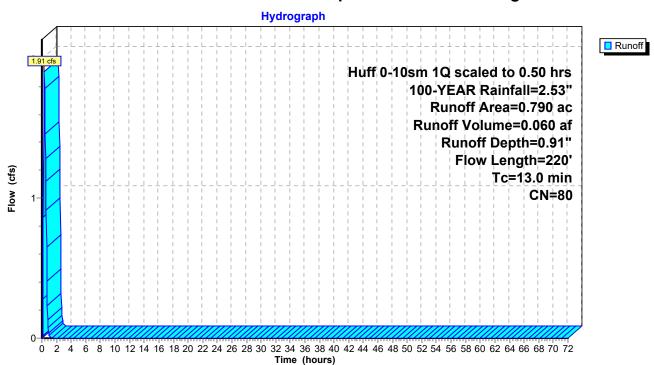
Summary for Subcatchment 1B: Pre-Developed Southeast Drainage Area

Runoff = 1.91 cfs @ 0.33 hrs, Volume= 0.060 af, Depth= 0.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 100-YEAR Rainfall=2.53"

_	Area	(ac) C	N Des	cription		
_	0.	790 8	30 >75°	% Grass c	over, Good	, HSG D
	0.	790	100.	.00% Pervi	ious Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	11.2	100	0.0160	0.15	,	Sheet Flow, Sheet Flow
	1.8	120	0.0240	1.08		Grass: Short n= 0.150 P2= 2.91" Shallow Concentrated Flow, Shallow Concentrated Flow Short Grass Pasture Kv= 7.0 fps
	13.0	220	Total			

Subcatchment 1B: Pre-Developed Southeast Drainage Area



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Summary for Subcatchment 2B: Post Developed Southeast Drainage Area (Detained)

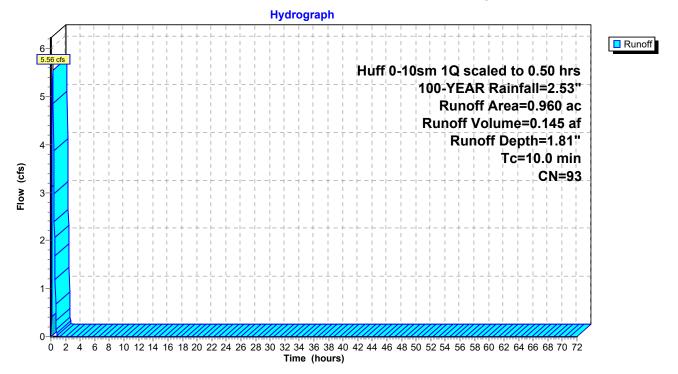
Runoff = 5.56 cfs @ 0.24 hrs, Volume= 0.145 af, Depth= 1.81"

Routed to Pond 4B: Southeast Basin

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 100-YEAR Rainfall=2.53"

	Area	(ac)	CN	Desc	cription		
	0.	260	80	>75%	√ Grass co	over, Good	, HSG D
	0.700 98 Paved parking, HSG D				ed parking	, HSG D	
	0.	960	93	Weig	hted Aver	age	
	0.	260		27.0	8% Pervio	us Area	
	0.700 72.92% Impervious Area			2% Imperv	∕ious Area		
	_		ci.	01	V/.1	0	December 1999
,		Leng		Slope	Velocity	Capacity	Description
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	10.0						Direct Entry, Direct Entry

Subcatchment 2B: Post Developed Southeast Drainage Area (Detained)



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Summary for Subcatchment 3B: Post Developed Southeast Drainage Direct Runoff

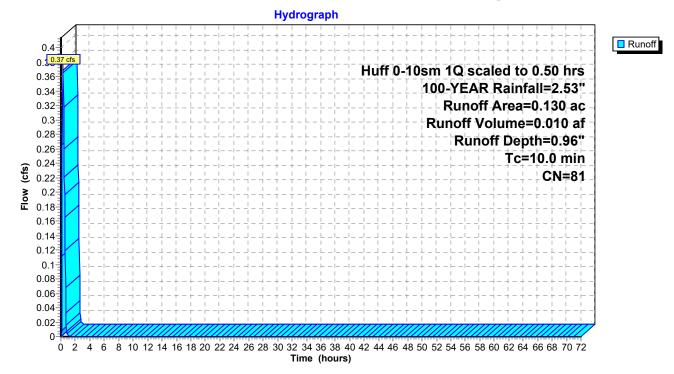
Runoff = 0.37 cfs @ 0.28 hrs, Volume= 0.010 af, Depth= 0.96" Routed to Link 5B : Final Southeast Outfall

Punoff by SCS TD 20 method LIU-SCS Weighted CN Time Span- 0.00.72

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Huff 0-10sm 1Q scaled to 0.50 hrs 100-YEAR Rainfall=2.53"

_	Area	(ac)	CN	Desc	ription		
	0.120 80 >75% Grass cover, Good					over, Good	, HSG D
	0.010 98 Paved parking, HSG D					HSG D	
	0.	130	81	Weig	hted Aver	age	
	0.	120		92.3	1% Pervio	us Area	
	0.010 7.69% Impervious Area			% Impervi	ous Area		
	_	_					
	Tc	Leng		Slope	Velocity	Capacity	Description
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	10.0						Direct Entry, Direct Entry

Subcatchment 3B: Post Developed Southeast Drainage Direct Runoff



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Summary for Pond 4B: Southeast Basin

Inflow Area = 0.960 ac, 72.92% Impervious, Inflow Depth = 1.81" for 100-YEAR event

Inflow 5.56 cfs @ 0.24 hrs. Volume= 0.145 af

Outflow 0.16 cfs @ 0.76 hrs, Volume= 0.145 af, Atten= 97%, Lag= 30.9 min

0.76 hrs, Volume= Primary 0.16 cfs @ 0.145 af

Routed to Link 5B: Final Southeast Outfall

Routing by Stor-Ind method. Time Span= 0.00-72.00 hrs. dt= 0.05 hrs. Peak Elev= 779.31' @ 0.76 hrs Surf.Area= 3,842 sf Storage= 5,970 cf

Plug-Flow detention time= 410.1 min calculated for 0.145 af (100% of inflow)

Center-of-Mass det. time= 409.6 min (429.5 - 19.9)

Volume	Inve	ert Avail.Sto	rage Storag	e Description	
#1	777.0	00' 14,2	36 cf Custor	m Stage Data (P	rismatic)Listed below (Recalc)
Elevatio (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
777.0	0	1,441	0	0	
778.0	0	2,390	1,916	1,916	
779.0	0	3,477	2,934	4,849	
780.0	0	4,669	4,073	8,922	
781.0	0	5,959	5,314	14,236	
Device	Routing	Invert	Outlet Devic	es	
#1	Primary	777.00'	12.0" Roun	nd Culvert L= 30	.0' Ke= 0.500
	·				776.00' S= 0.0333 '/' Cc= 0.900 ooth interior, Flow Area= 0.79 sf
#2	Device 1	777.00'		· ·	0.600 Limited to weir flow at low heads
#3	Device 1				ate X 6.00 columns
					24.0" Grate (42% open area)
				eir flow at low hea	

Primary OutFlow Max=0.16 cfs @ 0.76 hrs HW=779.31' (Free Discharge)

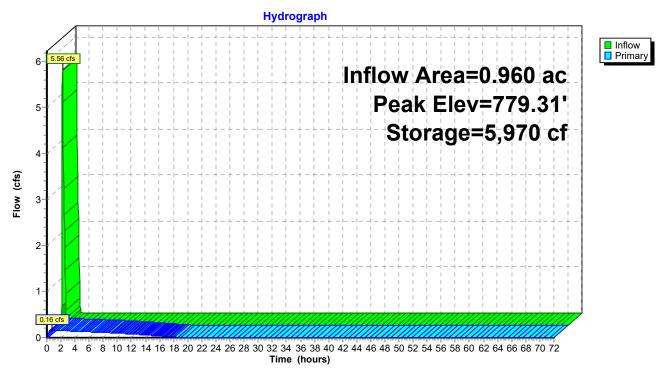
-1=Culvert (Passes 0.16 cfs of 5.08 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.16 cfs @ 7.18 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

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Pond 4B: Southeast Basin



Prepared by CESO, Inc.

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Summary for Link 5B: Final Southeast Outfall

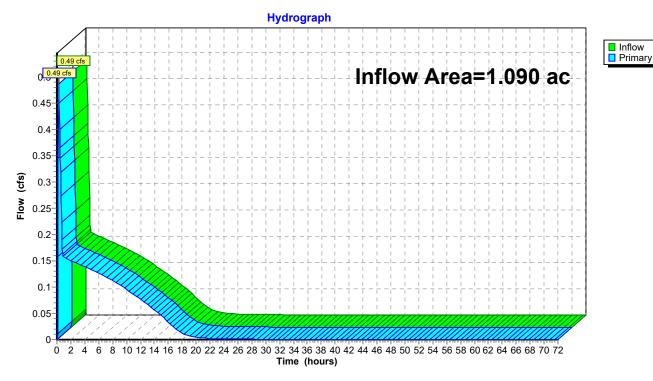
1.090 ac, 65.14% Impervious, Inflow Depth = 1.71" for 100-YEAR event Inflow Area =

Inflow 0.29 hrs, Volume= 0.155 af 0.49 cfs @

0.29 hrs, Volume= Primary 0.49 cfs @ 0.155 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 5B: Final Southeast Outfall





APPENDIX D: WATER QUALITY CALCULATIONS



APPENDIX D1.1: NORTHWEST DRAINAGE AREA WATER QUALITY CALCULATIONS

Hydrograph for Pond 4A: North Basin

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Primary (cfs)
0.00	0.00	2,022	776.06	0.01
0.25	0.00	2,015	776.06	0.01
0.50	0.00	2,009	776.06	0.01
0.75	0.00	2,003	776.06	0.01
1.00	0.00	1,997	776.06	0.01
1.25	0.00	1,991	776.06	0.01
1.50	0.00	1,985	776.06	0.01
1.75	0.00	1,980	776.06	0.01
2.00	0.00	1,974	776.06	0.01
2.25	0.00	1,968	776.06	0.01
2.50	0.00	1,962	776.06	0.01
2.75	0.00	1,956	776.06	0.01
3.00	0.00	1,950	776.06	0.01
3.25	0.00	1,944	776.06	0.01
3.50 3.75	0.00 0.00	1,939 1,933	776.06 776.06	0.01 0.01
4.00	0.00	1,933	776.06	0.01
4.25	0.00	1,922	776.06	0.01
4.50	0.00	1,916	776.06	0.01
4.75	0.00	1,910	776.06	0.01
5.00	0.00	1,905	776.06	0.01
5.25	0.00	1,899	776.06	0.01
5.50	0.00	1,894	776.06	0.01
5.75	0.00	1,888	776.06	0.01
6.00	0.00	1,883	776.06	0.01
6.25	0.00	1,877	776.06	0.01
6.50	0.00	1,872	776.06	0.01
6.75	0.00	1,866	776.06	0.01
7.00 7.25	0.00	1,861	776.06	0.01
7.25 7.50	0.00 0.00	1,856 1,850	776.06 776.05	0.01 0.01
7.75	0.00	1,845	776.05	0.01
8.00	0.00	1,840	776.05	0.01
8.25	0.00	1,834	776.05	0.01
8.50	0.00	1,829	776.05	0.01
8.75	0.00	1,824	776.05	0.01
9.00	0.00	1,819	776.05	0.01
9.25	0.00	1,813	776.05	0.01
9.50	0.00	1,808	776.05	0.01
9.75	0.00	1,803	776.05	0.01
10.00	0.00	1,798	776.05	0.01
10.25	0.00	1,793	776.05	0.01
10.50 10.75	0.00 0.00	1,788 1,783	776.05 776.05	0.01
11.00	0.00	1,778	776.05	0.01 0.01
11.25	0.00	1,773	776.05	0.01
11.50	0.00	1,768	776.05	0.01
11.75	0.00	1,763	776.05	0.01
12.00	0.00	1,758	776.05	0.01
12.25	0.00	1,753	776.05	0.01
12.50	0.00	1,748	776.05	0.01
12.75	0.00	1,743	776.05	0.01

Time	Inflow	Storage	Elevation	Primary
(hours)	(cfs)	(cubic-feet)	(feet)	(cfs)
13.00	0.00	1,738	776.05	0.01
13.25	0.00	1,733	776.05	0.01
13.50 13.75	0.00	1,729 1,724	776.05 776.05	0.01 0.01
14.00	0.00 0.00	1,724	776.05	0.01
14.25	0.00	1,714	776.05	0.01
14.50	0.00	1,710	776.05	0.01
14.75	0.00	1,705	776.05	0.01
15.00	0.00	1,700	776.05	0.01
15.25 15.50	0.00 0.00	1,696 1,691	776.05 776.05	0.01 0.01
15.75	0.00	1,686	776.05	0.01
16.00	0.00	1,682	776.05	0.01
16.25	0.00	1,677	776.05	0.01
16.50	0.00	1,673	776.05	0.01
16.75	0.00	1,668	776.05	0.01
17.00 17.25	0.00	1,664 1,659	776.05 776.05	0.01
17.23	0.00 0.00	1,655	776.05	0.00 0.00
17.75	0.00	1,650	776.05	0.00
18.00	0.00	1,646	776.05	0.00
18.25	0.00	1,641	776.05	0.00
18.50	0.00	1,637	776.05	0.00
18.75 19.00	0.00 0.00	1,632 1,628	776.05 776.05	0.00 0.00
19.00	0.00	1,624	776.05	0.00
19.50	0.00	1,619	776.05	0.00
19.75	0.00	1,615	776.05	0.00
20.00	0.00	1,611	776.05	0.00
20.25	0.00	1,607	776.05	0.00
20.50	0.00	1,602	776.05	0.00
20.75 21.00	0.00 0.00	1,598 1,594	776.05 776.05	0.00 0.00
21.25	0.00	1,590	776.05	0.00
21.50	0.00	1,586	776.05	0.00
21.75	0.00	1,581	776.05	0.00
22.00	0.00	1,577	776.05	0.00
22.25 22.50	0.00	1,573 1,569	776.05 776.05	0.00
22.75	0.00 0.00	1,565	776.05	0.00
23.00	0.00	1,561	776.05	0.00
23.25	0.00	1,557	776.05	0.00
23.50	0.00	1,553	776.05	0.00
23.75	0.00	1,549	776.05	0.00
24.00 24.25	0.00 0.00	1,545 1,541	776.05 776.05	0.00 0.00
24.50	0.00	1,537	776.05	0.00
24.75	0.00	1,533	776.05	0.00
25.00	0.00	1,529	776.05	0.00
25.25	0.00	1,525	776.05	0.00
25.50 25.75	0.00	1,521 1,517	776.05	0.00
25.75	0.00	1,517	776.05	0.00

Time	Inflow	Storage	Elevation	Primary
(hours)	(cfs)	(cubic-feet)	(feet)	(cfs)
26.00	0.00	1,514	776.04	0.00
26.25	0.00	1,510	776.04	0.00
26.50	0.00	1,506	776.04	0.00
26.75	0.00	1,502	776.04	0.00
27.00	0.00	1,498	776.04	0.00
27.25	0.00	1,495	776.04	0.00
27.50	0.00	1,491	776.04	0.00
27.75	0.00	1,487	776.04	0.00
28.00	0.00	1,483	776.04	0.00
28.25	0.00	1,480	776.04	0.00
28.50	0.00	1,476	776.04	0.00
28.75	0.00	1,472	776.04	0.00
29.00	0.00	1,469	776.04	0.00
29.25	0.00	1,465	776.04	0.00
29.50	0.00	1,461	776.04	0.00
29.75	0.00	1,458	776.04	0.00
30.00	0.00	1,454	776.04	0.00
30.25	0.00	1,451	776.04	0.00
30.50	0.00	1,447	776.04	0.00
30.75	0.00	1,443	776.04	0.00
31.00	0.00	1,440	776.04	0.00
31.25	0.00	1,436	776.04	0.00
31.50	0.00	1,433	776.04	0.00
31.75	0.00	1,429	776.04	0.00
32.00	0.00	1,426	776.04	0.00
32.25	0.00	1,423	776.04	0.00
32.50	0.00	1,419	776.04	0.00
32.75	0.00	1,416	776.04	0.00
33.00	0.00	1,412	776.04	0.00
33.25	0.00	1,409	776.04	0.00
33.50	0.00	1,406	776.04	0.00
33.75	0.00	1,402	776.04	0.00
34.00	0.00	1,399	776.04	0.00
34.25	0.00	1,396	776.04	0.00
34.50	0.00	1,392	776.04	0.00
34.75	0.00	1,389	776.04	0.00
35.00	0.00	1,386	776.04	0.00
35.25	0.00	1,382	776.04	0.00
35.50	0.00	1,379	776.04	0.00
35.75	0.00	1,376	776.04	0.00
36.00	0.00	1,373	776.04	0.00
36.25	0.00	1,369	776.04	0.00
36.50	0.00	1,366	776.04	0.00
36.75	0.00	1,363	776.04	0.00
37.00	0.00	1,360	776.04	0.00
37.25	0.00	1,357	776.04	0.00
37.50	0.00	1,354	776.04	0.00
37.75	0.00	1,350	776.04	0.00
38.00	0.00	1,347	776.04	0.00
38.25	0.00	1,344	776.04	0.00
38.50	0.00	1,341	776.04	0.00
38.75	0.00	1,338	776.04	0.00

Time	Inflow	Storage	Elevation	Primary
(hours)	(cfs)	(cubic-feet)	(feet)	(cfs)
39.00	0.00	1,335	776.04	0.00
39.25 39.50	0.00 0.00	1,332 1,329	776.04 776.04	0.00 0.00
39.75	0.00	1,329	776.04	0.00
40.00	0.00	1,323	776.04	0.00
40.25	0.00	1,320	776.04	0.00
40.50	0.00	1,317	776.04	0.00
40.75	0.00	1,314	776.04	0.00
41.00	0.00	1,311	776.04	0.00
41.25	0.00	1,308	776.04	0.00
41.50	0.00	1,305	776.04	0.00
41.75	0.00	1,302	776.04	0.00
42.00	0.00	1,299	776.04	0.00
42.25	0.00	1,297	776.04	0.00
42.50	0.00	1,294	776.04	0.00
42.75	0.00	1,291	776.04	0.00
43.00	0.00	1,288	776.04	0.00
43.25	0.00	1,285	776.04	0.00
43.50 43.75	0.00	1,282 1,279	776.04 776.04	0.00
44.00	0.00 0.00	1,279	776.04	0.00 0.00
44.25	0.00	1,274	776.04	0.00
44.50	0.00	1,271	776.04	0.00
44.75	0.00	1,268	776.04	0.00
45.00	0.00	1,266	776.04	0.00
45.25	0.00	1,263	776.04	0.00
45.50	0.00	1,260	776.04	0.00
45.75	0.00	1,257	776.04	0.00
46.00	0.00	1,255	776.04	0.00
46.25	0.00	1,252	776.04	0.00
46.50	0.00	1,249	776.04	0.00
46.75	0.00	1,247	776.04	0.00
47.00	0.00	1,244	776.04	0.00
47.25	0.00	1,241	776.04	0.00
47.50 47.75	0.00 0.00	1,239 1,236	776.04 776.04	0.00 0.00
48.00	0.00	1,234	776.04	0.00
48.25	0.00	1,231	776.04	0.00
48.50	0.00	1,228	776.04	0.00
48.75	0.00	1,226	776.04	0.00
49.00	0.00	1,223	776.04	0.00
49.25	0.00	1,221	776.04	0.00
49.50	0.00	1,218	776.04	0.00
49.75	0.00	1,216	776.04	0.00
50.00	0.00	1,213	776.04	0.00
50.25	0.00	1,211	776.04	0.00
50.50	0.00	1,208	776.04	0.00
50.75 51.00	0.00	1,206	776.04	0.00
51.00 51.25	0.00 0.00	1,203 1,201	776.04 776.04	0.00 0.00
51.50	0.00	1,198	776.04	0.00
51.75	0.00	1,196	776.04	0.00
J J	2.00	.,	0.0 1	0.00

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Primary (cfs)
52.00	0.00	1,193	776.04	0.00
52.25	0.00	1,191	776.04	0.00
52.50	0.00	1,189	776.04	0.00
52.75	0.00	1,186	776.04	0.00
53.00	0.00	1,184	776.04	0.00
53.25 53.50	0.00 0.00	1,181 1,179	776.04 776.04	0.00 0.00
53.75	0.00	1,179	776.04	0.00
54.00	0.00	1,174	776.03	0.00
54.25	0.00	1,172	776.03	0.00
54.50	0.00	1,170	776.03	0.00
54.75	0.00	1,167	776.03	0.00
55.00 55.25	0.00 0.00	1,165 1,163	776.03 776.03	0.00 0.00
55.50	0.00	1,163	776.03	0.00
55.75	0.00	1,158	776.03	0.00
56.00	0.00	1,156	776.03	0.00
56.25	0.00	1,154	776.03	0.00
56.50	0.00	1,151	776.03	0.00
56.75 57.00	0.00	1,149	776.03	0.00
57.00 57.25	0.00 0.00	1,147 1,145	776.03 776.03	0.00 0.00
57.50	0.00	1,143	776.03	0.00
57.75	0.00	1,140	776.03	0.00
58.00	0.00	1,138	776.03	0.00
58.25	0.00	1,136	776.03	0.00
58.50	0.00	1,134	776.03	0.00
58.75 59.00	0.00 0.00	1,132 1,130	776.03 776.03	0.00 0.00
59.25	0.00	1,127	776.03	0.00
59.50	0.00	1,125	776.03	0.00
59.75	0.00	1,123	776.03	0.00
60.00	0.00	1,121	776.03	0.00
60.25	0.00	1,119	776.03	0.00
60.50 60.75	0.00 0.00	1,117 1,115	776.03 776.03	0.00 0.00
61.00	0.00	1,113	776.03	0.00
61.25	0.00	1,111	776.03	0.00
61.50	0.00	1,109	776.03	0.00
61.75	0.00	1,107	776.03	0.00
62.00	0.00	1,105	776.03	0.00
62.25 62.50	0.00 0.00	1,103 1,101	776.03 776.03	0.00 0.00
62.75	0.00	1,099	776.03	0.00
63.00	0.00	1,097	776.03	0.00
63.25	0.00	1,095	776.03	0.00
63.50	0.00	1,093	776.03	0.00
63.75	0.00	1,091	776.03	0.00
64.00 64.25	0.00 0.00	1,089 1,087	776.03 776.03	0.00 0.00
64.50	0.00	1,085	776.03	0.00
64.75	0.00	1,083	776.03	0.00

Time	Inflow	Storage	Elevation	Primary
(hours)	(cfs)	(cubic-feet)	(feet)	(cfs)
65.00	0.00	1,081	776.03	0.00
65.25	0.00	1,079	776.03	0.00
65.50	0.00	1,077	776.03	0.00
65.75	0.00	1,075	776.03	0.00
66.00	0.00	1,073	776.03	0.00
66.25	0.00	1,071	776.03	0.00
66.50	0.00	1,070	776.03	0.00
66.75	0.00	1,068	776.03	0.00
67.00	0.00	1,066	776.03	0.00
67.25	0.00	1,064	776.03	0.00
67.50	0.00	1,062	776.03	0.00
67.75	0.00	1,060	776.03	0.00
68.00	0.00	1,058	776.03	0.00
68.25	0.00	1,057	776.03	0.00
68.50	0.00	1,055	776.03	0.00
68.75	0.00	1,053	776.03	0.00
69.00	0.00	1,051	776.03	0.00
69.25	0.00	1,049	776.03	0.00
69.50	0.00	1,048	776.03	0.00
69.75	0.00	1,046	776.03	0.00
70.00	0.00	1,044	776.03	0.00
70.25	0.00	1,042	776.03	0.00
70.50	0.00	1,041	776.03	0.00
70.75	0.00	1,039	776.03	0.00
71.00	0.00	1,037	776.03	0.00
71.25	0.00	1,035	776.03	0.00
71.50	0.00	1,034	776.03	0.00
71.75	0.00	1,032	776.03	0.00
72.00	0.00	1,030	776.03	0.00



APPENDIX D1.2: SOUTHEAST DRAINAGE AREA WATER QUALITY CALCULATIONS

Hydrograph for Pond 4B: Southeast Basin

Time	Inflow	Storage	Elevation	Primary
(hours)	(cfs)	(cubic-feet)	(feet)	(cfs)
0.00	0.00	458	777.29	0.05
0.25 0.50	0.00 0.00	416 377	777.27 777.24	0.04 0.04
0.50	0.00	341	777.22	0.04
1.00	0.00	307	777.20	0.04
1.25	0.00	276	777.18	0.03
1.50	0.00	248	777.16	0.03
1.75	0.00	223	777.15	0.03
2.00 2.25	0.00 0.00	201 181	777.13 777.12	0.02 0.02
2.23	0.00	165	777.12	0.02
2.75	0.00	150	777.10	0.02
3.00	0.00	137	777.09	0.01
3.25	0.00	126	777.09	0.01
3.50	0.00	117	777.08	0.01
3.75 4.00	0.00 0.00	109 101	777.07 777.07	0.01 0.01
4.00	0.00	94	777.06	0.01
4.50	0.00	88	777.06	0.01
4.75	0.00	83	777.06	0.01
5.00	0.00	78	777.05	0.01
5.25 5.50	0.00 0.00	74 70	777.05 777.05	0.00 0.00
5.75	0.00	66	777.05	0.00
6.00	0.00	63	777.04	0.00
6.25	0.00	60	777.04	0.00
6.50	0.00	58	777.04	0.00
6.75	0.00	55 53	777.04	0.00
7.00 7.25	0.00 0.00	53 51	777.04 777.03	0.00 0.00
7.50	0.00	49	777.03	0.00
7.75	0.00	47	777.03	0.00
8.00	0.00	45	777.03	0.00
8.25	0.00	43	777.03	0.00
8.50 9.75	0.00	41 39	777.03	0.00
8.75 9.00	0.00 0.00	38	777.03 777.03	0.00 0.00
9.25	0.00	36	777.02	0.00
9.50	0.00	35	777.02	0.00
9.75	0.00	33	777.02	0.00
10.00	0.00	32	777.02	0.00
10.25 10.50	0.00 0.00	31 29	777.02 777.02	0.00 0.00
10.30	0.00	28	777.02	0.00
11.00	0.00	27	777.02	0.00
11.25	0.00	26	777.02	0.00
11.50	0.00	25	777.02	0.00
11.75	0.00	24 23	777.02 777.02	0.00 0.00
12.00 12.25	0.00 0.00	23 22	777.02 777.01	0.00
12.50	0.00	21	777.01	0.00
12.75	0.00	20	777.01	0.00

Time	Inflow	Storage	Elevation	Primary
(hours)	(cfs)	(cubic-feet)	(feet)	(cfs)
13.00	0.00	19	777.01	0.00
13.25	0.00	18	777.01	0.00
13.50	0.00	18	777.01	0.00
13.75 14.00	0.00 0.00	17 16	777.01 777.01	0.00 0.00
14.00	0.00	16	777.01	0.00
14.50	0.00	15	777.01	0.00
14.75	0.00	14	777.01	0.00
15.00	0.00	14	777.01	0.00
15.25	0.00	13	777.01	0.00
15.50	0.00	13	777.01	0.00
15.75 16.00	0.00 0.00	12 12	777.01 777.01	0.00 0.00
16.25	0.00	11	777.01	0.00
16.50	0.00	11	777.01	0.00
16.75	0.00	10	777.01	0.00
17.00	0.00	10	777.01	0.00
17.25	0.00	9	777.01	0.00
17.50 17.75	0.00 0.00	9	777.01 777.01	0.00 0.00
18.00	0.00	8	777.01	0.00
18.25	0.00	8	777.01	0.00
18.50	0.00	8	777.01	0.00
18.75	0.00	7	777.00	0.00
19.00	0.00	7	777.00	0.00
19.25	0.00	7 6	777.00	0.00
19.50 19.75	0.00 0.00	6	777.00 777.00	0.00 0.00
20.00	0.00	6	777.00	0.00
20.25	0.00	6	777.00	0.00
20.50	0.00	5	777.00	0.00
20.75	0.00	5	777.00	0.00
21.00	0.00	5 5	777.00	0.00
21.25 21.50	0.00 0.00	5	777.00 777.00	0.00 0.00
21.75	0.00	4	777.00	0.00
22.00	0.00	4	777.00	0.00
22.25	0.00	4	777.00	0.00
22.50	0.00	4	777.00	0.00
22.75	0.00	4	777.00	0.00
23.00 23.25	0.00 0.00	4 3	777.00 777.00	0.00 0.00
23.50	0.00	3	777.00	0.00
23.75	0.00	3	777.00	0.00
24.00	0.00	3	777.00	0.00
24.25	0.00	3	777.00	0.00
24.50 24.75	0.00	3	777.00 777.00	0.00
24.75 25.00	0.00 0.00	3 3	777.00	0.00 0.00
25.25	0.00	2	777.00	0.00
25.50	0.00	2 2 2	777.00	0.00
25.75	0.00	2	777.00	0.00

Time	Inflow	Storage	Elevation	Primary
(hours)	(cfs)	(cubic-feet)	(feet)	(cfs)
26.00	0.00	2	777.00	0.00
26.25	0.00	2	777.00	0.00
26.50	0.00	2	777.00	0.00
26.75	0.00	2	777.00	0.00
27.00	0.00	2	777.00	0.00
27.25	0.00	2	777.00	0.00
27.50	0.00	2	777.00	0.00
27.75	0.00	2 2	777.00	0.00
28.00	0.00		777.00	0.00
28.25	0.00	1	777.00	0.00
28.50	0.00	1	777.00	0.00
28.75	0.00	1 1	777.00	0.00
29.00 29.25	0.00 0.00	1	777.00 777.00	0.00 0.00
29.23	0.00	1	777.00	0.00
29.75	0.00	1	777.00	0.00
30.00	0.00	1	777.00	0.00
30.25	0.00	1	777.00	0.00
30.50	0.00	1	777.00	0.00
30.75	0.00	1	777.00	0.00
31.00	0.00	1	777.00	0.00
31.25	0.00	1	777.00	0.00
31.50	0.00	1	777.00	0.00
31.75	0.00	1	777.00	0.00
32.00	0.00	1	777.00	0.00
32.25	0.00	1	777.00	0.00
32.50	0.00	1	777.00	0.00
32.75	0.00	1	777.00	0.00
33.00	0.00	1	777.00	0.00
33.25	0.00	1	777.00	0.00
33.50	0.00	1	777.00	0.00
33.75	0.00	1	777.00	0.00
34.00	0.00	1	777.00	0.00
34.25	0.00	1	777.00	0.00
34.50	0.00	1	777.00	0.00
34.75	0.00 0.00	0	777.00	0.00
35.00 35.25		0	777.00 777.00	0.00
35.50	0.00 0.00	0	777.00	0.00 0.00
35.75	0.00	0	777.00	0.00
36.00	0.00	0	777.00	0.00
36.25	0.00	0	777.00	0.00
36.50	0.00	Ő	777.00	0.00
36.75	0.00	0	777.00	0.00
37.00	0.00	0	777.00	0.00
37.25	0.00	0	777.00	0.00
37.50	0.00	0	777.00	0.00
37.75	0.00	0	777.00	0.00
38.00	0.00	0	777.00	0.00
38.25	0.00	0	777.00	0.00
38.50	0.00	0	777.00	0.00
38.75	0.00	0	777.00	0.00

T:	la fla	Ctara ra	Classation	Duine
Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Primary (cfs)
39.00	0.00	0	777.00	0.00
39.25	0.00	0	777.00	0.00
39.50	0.00	0	777.00	0.00
39.75	0.00	0	777.00	0.00
40.00	0.00	0	777.00	0.00
40.25	0.00	0	777.00	0.00
40.50	0.00	0	777.00	0.00
40.75 41.00	0.00 0.00	0	777.00 777.00	0.00 0.00
41.00	0.00	0	777.00	0.00
41.50	0.00	0	777.00	0.00
41.75	0.00	0	777.00	0.00
42.00	0.00	Ö	777.00	0.00
42.25	0.00	0	777.00	0.00
42.50	0.00	0	777.00	0.00
42.75	0.00	0	777.00	0.00
43.00	0.00	0	777.00	0.00
43.25	0.00	0	777.00	0.00
43.50	0.00	0	777.00	0.00
43.75	0.00	0	777.00	0.00
44.00 44.25	0.00	0	777.00	0.00
44.25 44.50	0.00 0.00	0	777.00 777.00	0.00 0.00
44.75	0.00	0	777.00	0.00
45.00	0.00	Ö	777.00	0.00
45.25	0.00	Ö	777.00	0.00
45.50	0.00	0	777.00	0.00
45.75	0.00	0	777.00	0.00
46.00	0.00	0	777.00	0.00
46.25	0.00	0	777.00	0.00
46.50	0.00	0	777.00	0.00
46.75	0.00	0	777.00	0.00
47.00	0.00	0	777.00	0.00
47.25	0.00	0	777.00 777.00	0.00
47.50 47.75	0.00 0.00	0 0	777.00	0.00 0.00
48.00	0.00	0	777.00	0.00
48.25	0.00	Ő	777.00	0.00
48.50	0.00	0	777.00	0.00
48.75	0.00	0	777.00	0.00
49.00	0.00	0	777.00	0.00
49.25	0.00	0	777.00	0.00
49.50	0.00	0	777.00	0.00
49.75	0.00	0	777.00	0.00
50.00	0.00	0	777.00	0.00
50.25	0.00	0	777.00	0.00
50.50 50.75	0.00 0.00	0 0	777.00 777.00	0.00 0.00
50.75	0.00	0	777.00	0.00
51.00	0.00	0	777.00	0.00
51.50	0.00	Ö	777.00	0.00
51.75	0.00	Ö	777.00	0.00

Time	Inflow	Ctorogo	Clayation	Drimon
Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Primary (cfs)
52.00	0.00	0	777.00	0.00
52.25	0.00	0	777.00	0.00
52.50	0.00	0	777.00	0.00
52.75	0.00	0	777.00	0.00
53.00	0.00	0	777.00	0.00
53.25	0.00	0	777.00	0.00
53.50	0.00	0	777.00	0.00
53.75 54.00	0.00 0.00	0	777.00 777.00	0.00 0.00
54.00 54.25	0.00	0	777.00	0.00
54.50	0.00	0	777.00	0.00
54.75	0.00	0	777.00	0.00
55.00	0.00	0	777.00	0.00
55.25	0.00	0	777.00	0.00
55.50	0.00	0	777.00	0.00
55.75	0.00	0	777.00	0.00
56.00	0.00	0	777.00	0.00
56.25	0.00	0	777.00	0.00
56.50	0.00	0	777.00	0.00
56.75 57.00	0.00	0	777.00	0.00
57.00 57.25	0.00 0.00	0	777.00 777.00	0.00 0.00
57.25 57.50	0.00	0	777.00	0.00
57.75	0.00	0	777.00	0.00
58.00	0.00	Ö	777.00	0.00
58.25	0.00	0	777.00	0.00
58.50	0.00	0	777.00	0.00
58.75	0.00	0	777.00	0.00
59.00	0.00	0	777.00	0.00
59.25	0.00	0	777.00	0.00
59.50	0.00	0	777.00	0.00
59.75	0.00	0	777.00	0.00
60.00 60.25	0.00 0.00	0	777.00 777.00	0.00 0.00
60.50	0.00	0	777.00	0.00
60.75	0.00	Ö	777.00	0.00
61.00	0.00	0	777.00	0.00
61.25	0.00	0	777.00	0.00
61.50	0.00	0	777.00	0.00
61.75	0.00	0	777.00	0.00
62.00	0.00	0	777.00	0.00
62.25	0.00	0	777.00	0.00
62.50	0.00	0	777.00	0.00
62.75	0.00	0	777.00	0.00
63.00 63.25	0.00 0.00	0	777.00 777.00	0.00 0.00
63.50	0.00	0	777.00	0.00
63.75	0.00	Ö	777.00	0.00
64.00	0.00	Ö	777.00	0.00
64.25	0.00	0	777.00	0.00
64.50	0.00	0	777.00	0.00
64.75	0.00	0	777.00	0.00

Time	Inflow	Storage	Elevation	Primary
(hours)	(cfs)	(cubic-feet)	(feet)	(cfs)
65.00	0.00	0	777.00	0.00
65.25	0.00	0	777.00	0.00
65.50	0.00	0	777.00	0.00
65.75	0.00	0	777.00	0.00
66.00	0.00	0	777.00	0.00
66.25	0.00	0	777.00	0.00
66.50	0.00	0	777.00	0.00
66.75	0.00	0	777.00	0.00
67.00	0.00	0	777.00	0.00
67.25	0.00	0	777.00	0.00
67.50	0.00	0	777.00	0.00
67.75	0.00	0	777.00	0.00
68.00	0.00	0	777.00	0.00
68.25	0.00	0	777.00	0.00
68.50	0.00	0	777.00	0.00
68.75	0.00	0	777.00	0.00
69.00	0.00	0	777.00	0.00
69.25	0.00	0	777.00	0.00
69.50	0.00	0	777.00	0.00
69.75	0.00	0	777.00	0.00
70.00	0.00	0	777.00	0.00
70.25	0.00	0	777.00	0.00
70.50	0.00	0	777.00	0.00
70.75	0.00	0	777.00	0.00
71.00	0.00	0	777.00	0.00
71.25	0.00	0	777.00	0.00
71.50	0.00	0	777.00	0.00
71.75	0.00	0	777.00	0.00
72.00	0.00	0	777.00	0.00



APPENDIX F: SITE SOILS



NRCS

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Johnson County, Indiana



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

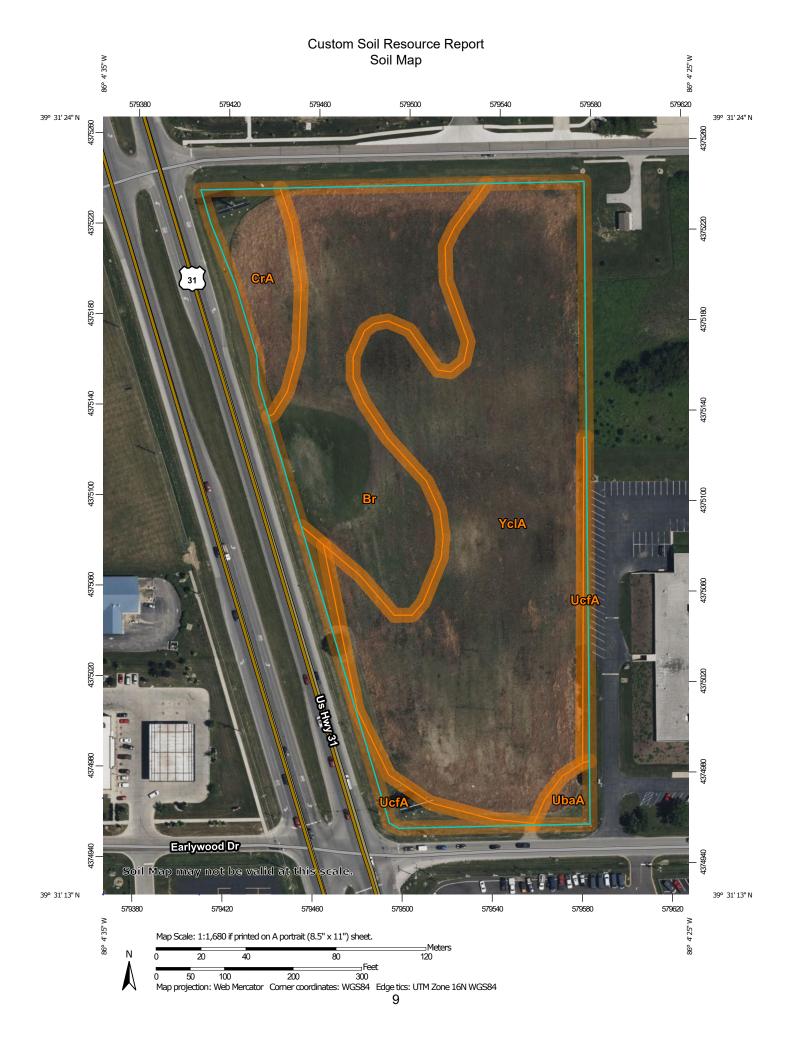
Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons



Soil Map Unit Lines



Soil Map Unit Points

Special Point Features

ဖ

Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot

Landfill Lava Flow



Marsh or swamp

Mine or Quarry

Miscellaneous Water Perennial Water

Rock Outcrop

Saline Spot

Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

Spoil Area



Stony Spot Very Stony Spot



Wet Spot



Other

Special Line Features

Water Features

Streams and Canals

Transportation

Rails

Interstate Highways

US Routes

Major Roads

00

Local Roads

Background

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15.800.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Johnson County, Indiana Survey Area Data: Version 32, Aug 26, 2024

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Jun 15, 2022—Jun 21. 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
Br	Brookston silty clay loam, 0 to 2 percent slopes	2.5	27.9%
CrA	Crosby silt loam, fine-loamy subsoil, 0 to 2 percent slopes	0.6	6.8%
UbaA	Urban land-Brookston complex, 0 to 2 percent slopes	0.1	1.3%
UcfA	Urban land-Crosby silt loam complex, fine-loamy subsoil, 0 to 2 percent slopes	0.3	3.6%
YclA	Crosby silt loam, fine-loamy subsoil-Urban land complex, 0 to 2 percent slopes	5.5	60.4%
Totals for Area of Interest		9.1	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it

was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Johnson County, Indiana

Br—Brookston silty clay loam, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2t98n Elevation: 600 to 1,260 feet

Mean annual precipitation: 37 to 46 inches Mean annual air temperature: 48 to 55 degrees F

Frost-free period: 145 to 180 days

Farmland classification: Prime farmland if drained

Map Unit Composition

Brookston and similar soils: 95 percent

Minor components: 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Brookston

Setting

Landform: Till plains, depressions

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Dip Down-slope shape: Linear, concave

Across-slope shape: Concave

Parent material: Loess over loamy till

Typical profile

Ap - 0 to 16 inches: silty clay loam Btg1 - 16 to 32 inches: silty clay loam

Btg2 - 32 to 44 inches: loam C - 44 to 60 inches: loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20

to 0.60 in/hr)

Depth to water table: About 0 to 12 inches

Frequency of flooding: None Frequency of ponding: Frequent

Calcium carbonate, maximum content: 40 percent

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm) Available water supply, 0 to 60 inches: Moderate (about 8.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: B/D

Ecological site: F111XA007IN - Till Depression Flatwood

Hydric soil rating: Yes

Minor Components

Crosby

Percent of map unit: 5 percent

Landform: Till plains

Landform position (two-dimensional): Summit, footslope

Landform position (three-dimensional): Talf

Down-slope shape: Concave Across-slope shape: Linear

Ecological site: F111XA008IN - Wet Till Ridge

Hydric soil rating: No

CrA—Crosby silt loam, fine-loamy subsoil, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2thy4 Elevation: 600 to 1.000 feet

Mean annual precipitation: 36 to 44 inches
Mean annual air temperature: 49 to 54 degrees F

Frost-free period: 145 to 180 days

Farmland classification: Prime farmland if drained

Map Unit Composition

Crosby and similar soils: 93 percent Minor components: 7 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Crosby

Setting

Landform: Ground moraines, recessionial moraines, water-lain moraines Landform position (two-dimensional): Summit, backslope, footslope

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Silty material or loess over loamy till

Typical profile

Ap - 0 to 10 inches: silt loam

Btg - 10 to 17 inches: silty clay loam

2Bt - 17 to 29 inches: clay loam

2BCt - 29 to 36 inches: loam

2Cd - 36 to 79 inches: loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: 24 to 40 inches to densic material

Drainage class: Somewhat poorly drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Low to moderately high

(0.01 to 0.20 in/hr)

Depth to water table: About 6 to 24 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 55 percent

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm) Available water supply, 0 to 60 inches: Moderate (about 6.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: C/D

Ecological site: F111XA008IN - Wet Till Ridge

Hydric soil rating: No

Minor Components

Williamstown, moderately eroded

Percent of map unit: 5 percent

Landform: Water-lain moraines, ground moraines, recessionial moraines Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Linear, convex Ecological site: F111XA009IN - Till Ridge

Hydric soil rating: No

Treaty, drained

Percent of map unit: 2 percent

Landform: Depressions, water-lain moraines, swales Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Linear Across-slope shape: Concave

Ecological site: F111XA007IN - Till Depression Flatwood

Hydric soil rating: Yes

UbaA—Urban land-Brookston complex, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2y48h

Elevation: 640 to 930 feet

Mean annual precipitation: 36 to 42 inches Mean annual air temperature: 49 to 53 degrees F

Frost-free period: 175 to 185 days

Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 60 percent

Brookston, drained, and similar soils: 40 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Urban Land

Setting

Landform: Till plains

Description of Brookston, Drained

Setting

Landform: Depressions on till plains

Landform position (two-dimensional): Footslope

Down-slope shape: Concave Across-slope shape: Linear

Parent material: Loess over loamy till

Typical profile

H1 - 0 to 14 inches: silty clay loam H2 - 14 to 54 inches: clay loam H3 - 54 to 60 inches: loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20

to 0.60 in/hr)

Depth to water table: About 0 to 12 inches

Frequency of flooding: None Frequency of ponding: Frequent

Calcium carbonate, maximum content: 40 percent

Available water supply, 0 to 60 inches: High (about 9.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: B/D

Ecological site: F111XA007IN - Till Depression Flatwood

Hydric soil rating: Yes

UcfA—Urban land-Crosby silt loam complex, fine-loamy subsoil, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2y47p Elevation: 600 to 1,260 feet

Mean annual precipitation: 36 to 46 inches
Mean annual air temperature: 48 to 55 degrees F

Frost-free period: 145 to 180 days

Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 60 percent

Crosby and similar soils: 35 percent Minor components: 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Crosby

Setting

Landform: Water-lain moraines, ground moraines, recessionial moraines Landform position (two-dimensional): Summit, backslope, footslope

Landform position (three-dimensional): Interfluve, rise

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Silty material or loess over loamy till

Typical profile

Ap - 0 to 8 inches: silt loam BE - 8 to 11 inches: silt loam Bt - 11 to 14 inches: silt loam 2Bt - 14 to 28 inches: silty clay 2BCt - 28 to 36 inches: loam 2Cd - 36 to 79 inches: loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: 24 to 40 inches to densic material

Drainage class: Somewhat poorly drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Low to moderately high

(0.01 to 0.20 in/hr)

Depth to water table: About 6 to 24 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 50 percent

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 5.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: C/D

Ecological site: F111XA008IN - Wet Till Ridge

Hydric soil rating: No

Minor Components

Treaty, drained

Percent of map unit: 5 percent

Landform: Depressions, water-lain moraines, swales Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope, dip

Down-slope shape: Linear Across-slope shape: Concave

Ecological site: F111XA007IN - Till Depression Flatwood

Hydric soil rating: Yes

YclA—Crosby silt loam, fine-loamy subsoil-Urban land complex, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2w57p Elevation: 600 to 1,040 feet

Mean annual precipitation: 36 to 46 inches
Mean annual air temperature: 48 to 55 degrees F

Frost-free period: 145 to 180 days

Farmland classification: Not prime farmland

Map Unit Composition

Crosby and similar soils: 60 percent

Urban land: 30 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Crosby

Setting

Landform: Water-lain moraines, ground moraines, recessionial moraines Landform position (two-dimensional): Summit, backslope, footslope

Landform position (three-dimensional): Interfluve, rise

Down-slope shape: Linear, convex Across-slope shape: Convex, linear

Parent material: Silty material or loess over loamy till

Typical profile

Ap - 0 to 10 inches: silt loam

Btg - 10 to 17 inches: silty clay loam 2Bt - 17 to 29 inches: clay loam 2BCt - 29 to 36 inches: loam 2Cd - 36 to 79 inches: loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: 24 to 40 inches to densic material

Drainage class: Somewhat poorly drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Low to moderately high

(0.01 to 0.20 in/hr)

Depth to water table: About 6 to 24 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 55 percent

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm) Available water supply, 0 to 60 inches: Moderate (about 6.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: C/D

Ecological site: F111XA008IN - Wet Till Ridge

Hydric soil rating: No

Minor Components

Treaty, drained

Percent of map unit: 5 percent

Landform: Depressions, water-lain moraines, swales Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope, dip

Down-slope shape: Linear Across-slope shape: Concave

Ecological site: F111XA007IN - Till Depression Flatwood

Hydric soil rating: Yes

Williamstown, eroded

Percent of map unit: 5 percent

Landform: Water-lain moraines, ground moraines, recessionial moraines

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest,

rise

Down-slope shape: Convex, linear Across-slope shape: Linear, convex Ecological site: F111XA009IN - Till Ridge

Hydric soil rating: No

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